

DRILL HOLE LOG

DRILL HOLE No: BH 2

Hole Location:

SHEET 2 OF 2

PROJECT: JACKS POINT - HENLEY DOWNS

LOCATION: WOODSATED ROAD, QUEENSTOWN JOB No: 880054

CO-ORDINATES mN
mE

DRILL TYPE: UDR 650

HOLE STARTED: 10/10/2007

DATUM:

HOLE FINISHED: 10/10/2007

DIRECTION: N/A °
ANGLE FROM HORIZ.: 90°, vertical

R.L. GROUND: m

DRILLED BY: McNEILL DRILLING

R.L. COLLAR: m

LOGGED BY: SCW CHECKED:

| DESCRIPTION OF CORE | | | | | | | | | | S.P.T. Logs | | | | | | | | | | | | |
|---------------------|--|-----------------|----|----|---------------|----|----|--------------------------|----------------------|-----------------------|-------------|-----------|-------------|------------|--|--|--------------|---------|-------|----------------------|---|-----------------|
| GEOLOGICAL UNIT | ROCK OR SOIL TYPE, WEATHERING, HARDNESS, STRENGTH, COLOUR, LITHOLOGICAL FEATURES (bedding, cement, foliation, mineralogy, texture, etc...); | ROCK WEATHERING | | | ROCK STRENGTH | | | PT LOAD / UCS TEST (MPa) | CORE LOSS / LIFT (%) | METHOD, CORE & CASING | TEST SYMBOL | DEPTH (m) | GRAPHIC LOG | DEFECT LOG | FRACTURE LOG spacing of natural fractures (cm) | SIGNIFICANT JOINTS, BEDDING, CRUSHED AND SHEARED ZONES/SEAMS | DATE / DEPTH | RQD (%) | WATER | DRILL WATER LOSS (%) | SPT RESULTS | CORE BOX RL (m) |
| | | UW | SW | MW | HW | R4 | R3 | | | | | | | | | | | | | | | |
| Label Deposits | gravel. 9.5-10.0 = no sands and PP < 50kPa, SILT, dry, sl. plast, stiff very stiff pp = 50-150kPa, occasional rounded fine gravel, becoming more clayey. 10.0-11.0m (0.3m loss) contact. | | | | | | | | | HQT | 11 | X | | | | contact | | | | | SPT @ 11.0m 6, 7, 9, 10, 11, 7 n = 50 fr 265mm | |
| | Core Run ⇒ 11.0-12.4m 11.0-11.5m pp = 50-150kPa grey brown SILT with minor clay + occasional sandy lenses 11.5-12.0m pp = 350kPa, silty SAND (f-c) with minor clay, sl. plast. thinly laminated 12.0-12.4m pp = 50-100kPa silty SAND, non plastic, non cohesive, laminated. (no loss) | | | | | | | | | SPT | 12 | X | | | | | | | | | SPT @ 12.4m 10, 26, 19 n = 50 fr 70mm | |
| GLACIAL TILL | core ends at 12.4m | | | | | | | | | SPT | 13 | X | | | | | | | | | SPT @ 13.5m 5, 12, 15, 8 n = 50 fr 150mm | |
| | D.C. = SAND | | | | | | | | | HQT | 14 | X | | | | | | | | | SPT @ 15.0m 3, 5, 6, 7, 7, 7 n = 27 | |
| | D.C. = GRAVEL | | | | | | | | | SPT | 15 | X | | | | | | | | | | |
| | D.C. = GRAVEL | | | | | | | | | | 16 | | | | | | | | | | | |
| | END OF DRILLHOLE @ 15.45m. | | | | | | | | | | 17 | | | | | | | | | | | |
| | | | | | | | | | | | 18 | | | | | | | | | | | |
| | | | | | | | | | | | 19 | | | | | | | | | | | |

pp = pocket penetrometer test
D.C. = Driller's comment.

↑ SPT = standard penetration test
HQT = core drilling.

Appendix D: CPT Logs

CPT ANALYSIS NOTES

Soil Type

Interpretation using chart of Robertson & Campanella (1983). This is a simple but well proven interpretation using cone tip resistance (q_c) and friction ratio (f_R) only. No normalisation for overburden stress is applied. Cone tip resistance measured with the piezocone is corrected with measured pore pressure (u_c).

| | |
|---|-------------------|
|  | sand (and gravel) |
|  | silt-sand |
|  | silt |
|  | clay-silt |
|  | clay |
|  | peat |

Liquefaction Screening

The purpose of the screening is to highlight susceptible soils, that is sand and silt-sand in a relatively loose condition. This is not a full liquefaction risk assessment which requires knowledge of the particular earthquake risk at a site and additional analysis. The screening is based on the chart of Shibata and Teparaksa (1988).

| | |
|---|-----------------------|
|  | high susceptibility |
|  | medium susceptibility |
|  | low susceptibility |

High susceptibility is here defined as requiring a shear stress ratio of 0.2 to cause liquefaction with D_{50} for sands assumed to be 0.25 mm and for silty sands to be 0.05 mm.

Medium susceptibility is here defined as requiring a shear stress ratio of 0.4 to cause liquefaction with D_{50} for sands assumed to be 0.25 mm and for silty sands to be 0.05 mm.

Low susceptibility is all other cases.

Relative Density (D_R)

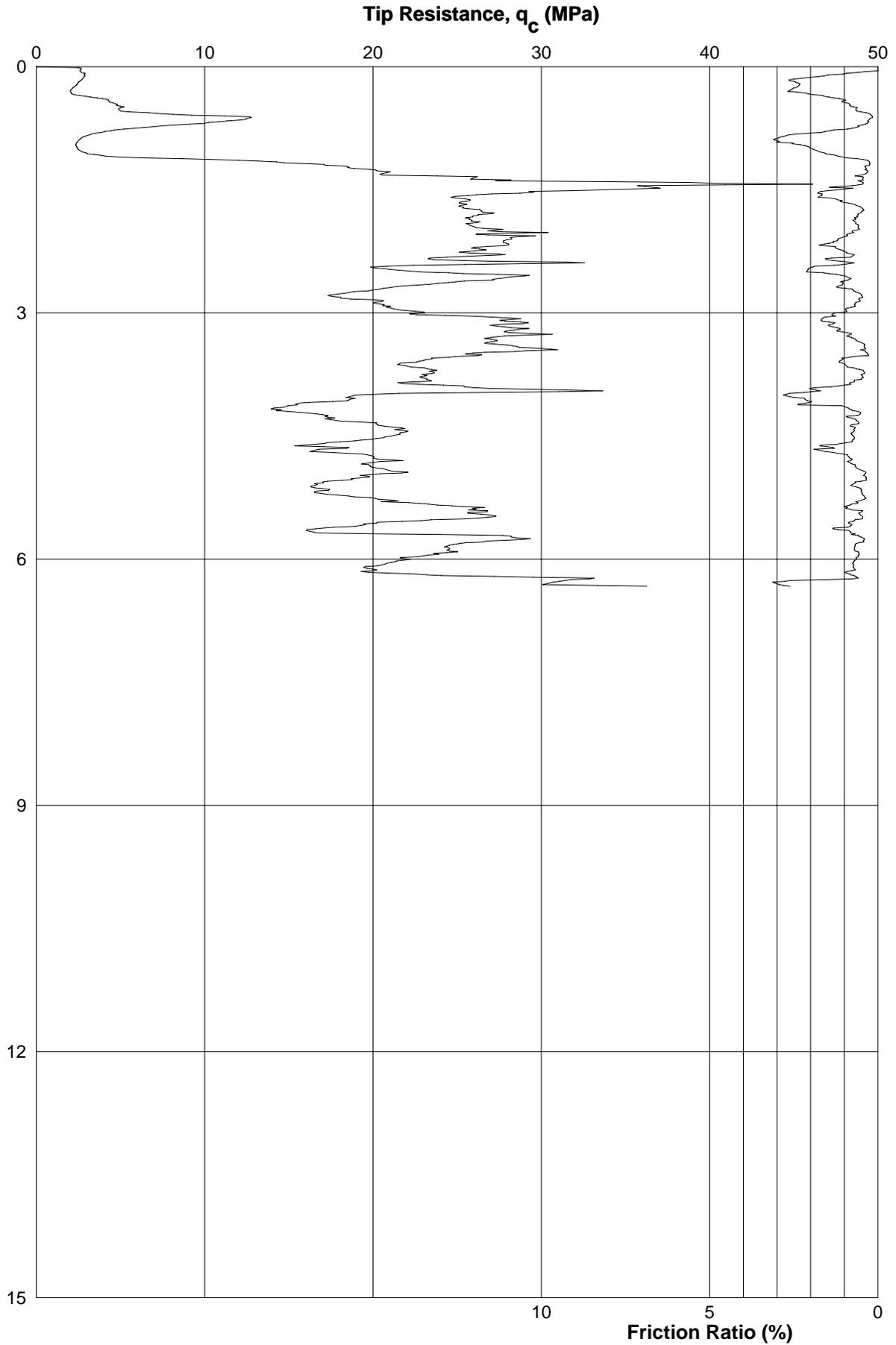
Based on the method of Baldi et. al. (1986) from data on normally consolidated sand.

Undrained Shear Strength (S_u)

Derived from the bearing capacity equation using $S_u = (q_c - \sigma_{vo})/15$.



STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 201

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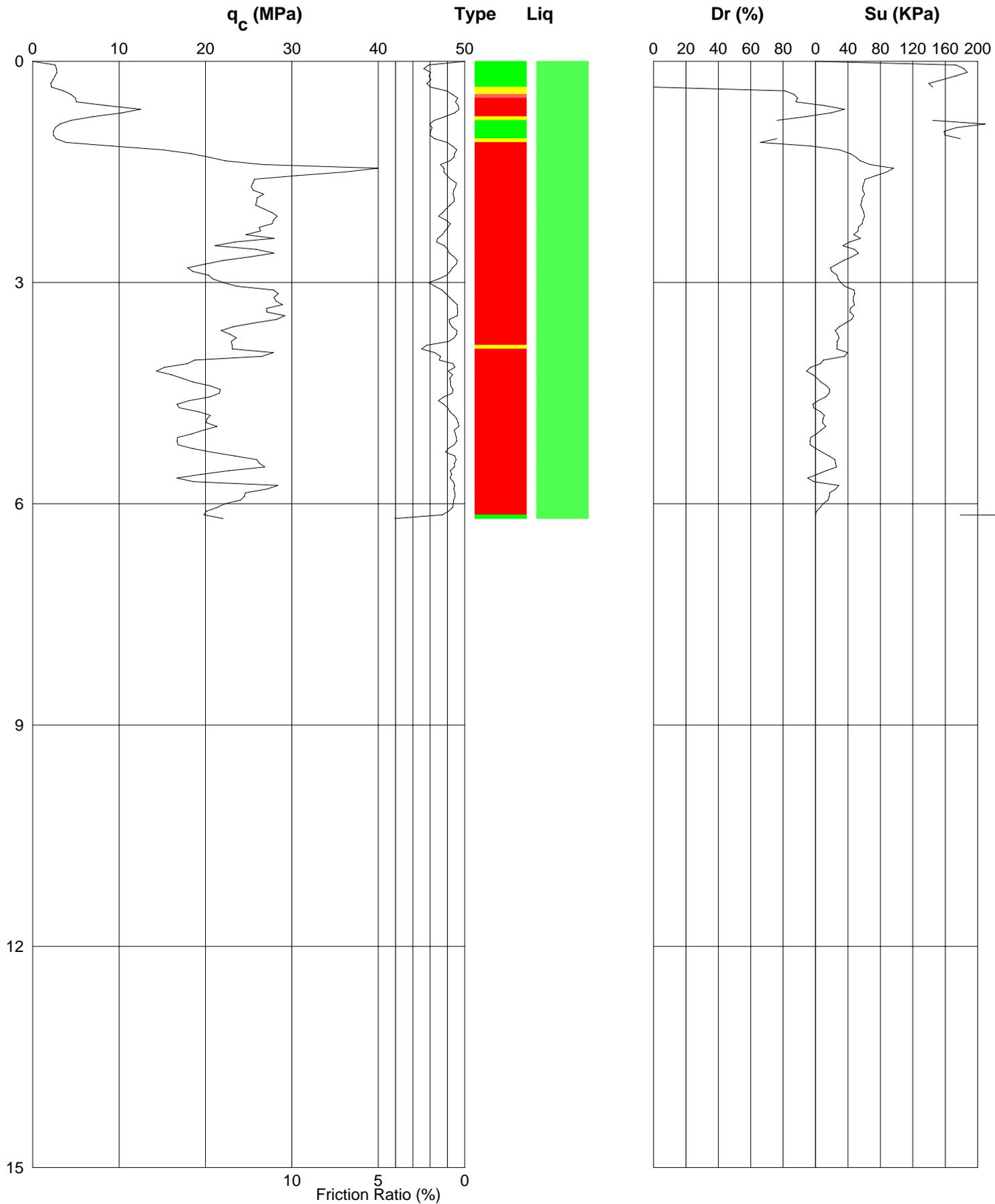
Location: Jacks Point, Queenstown

Date: 26-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

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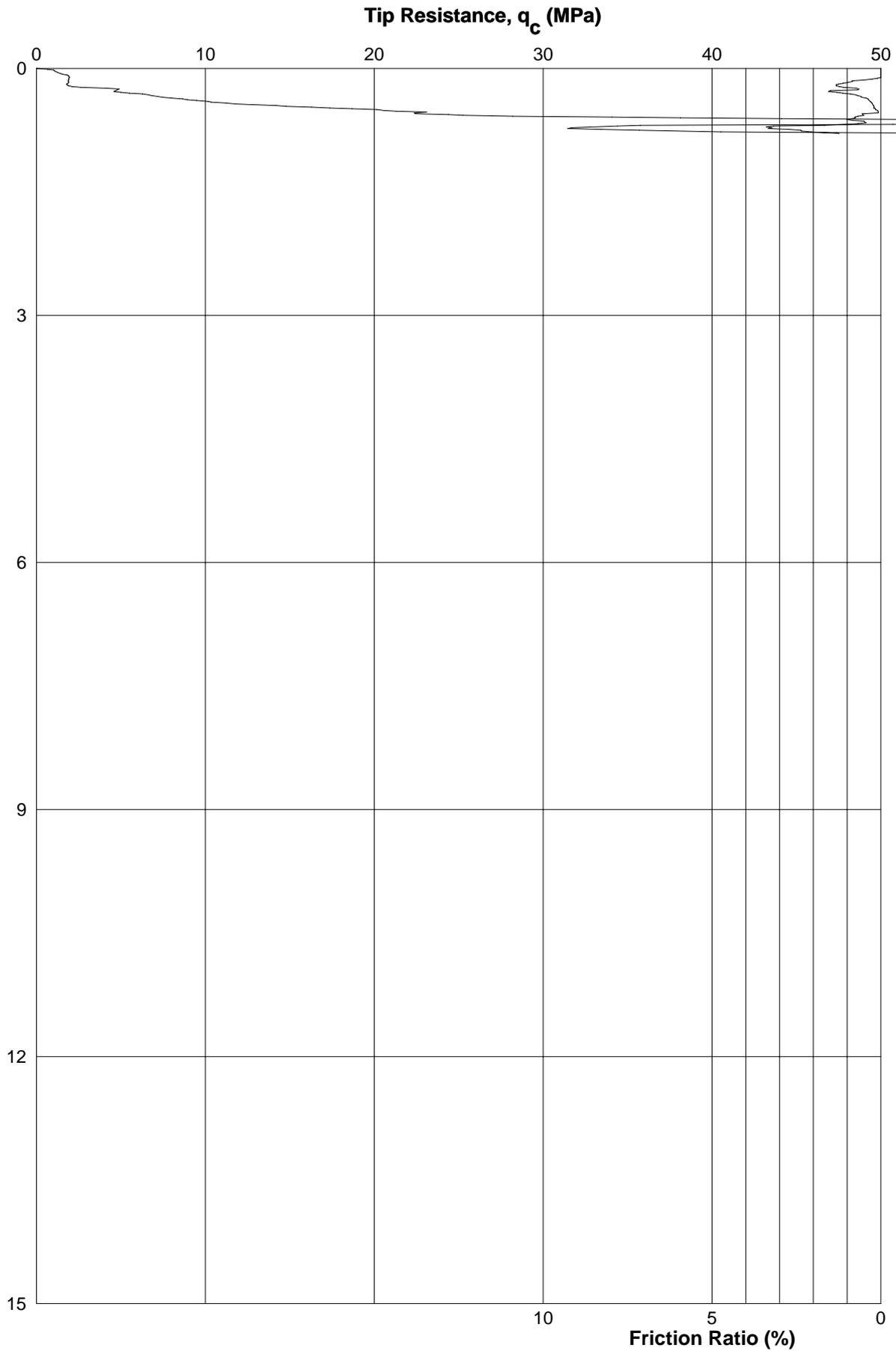
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Job No: 4934

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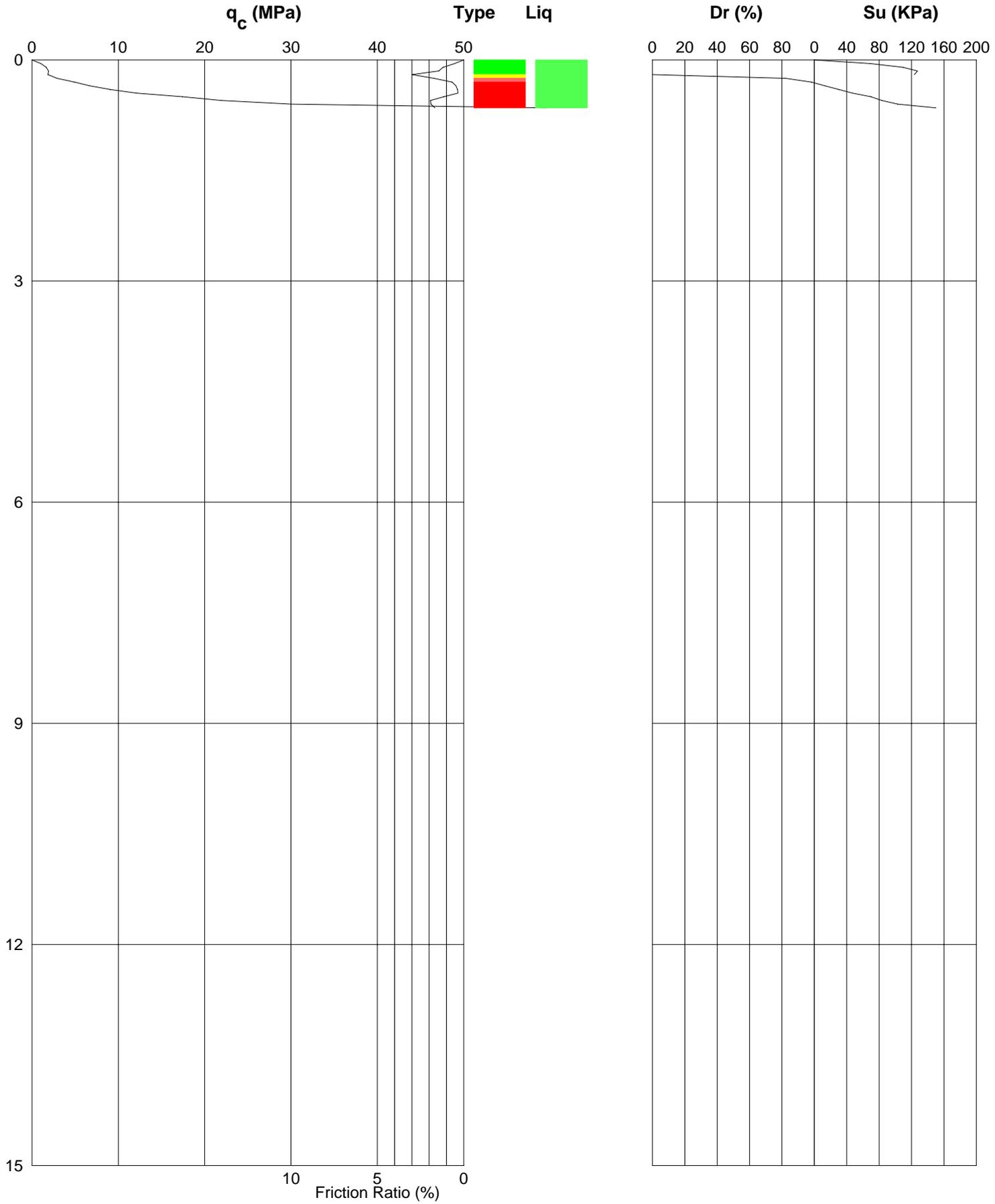
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Job No: 4934

CPT No: 202

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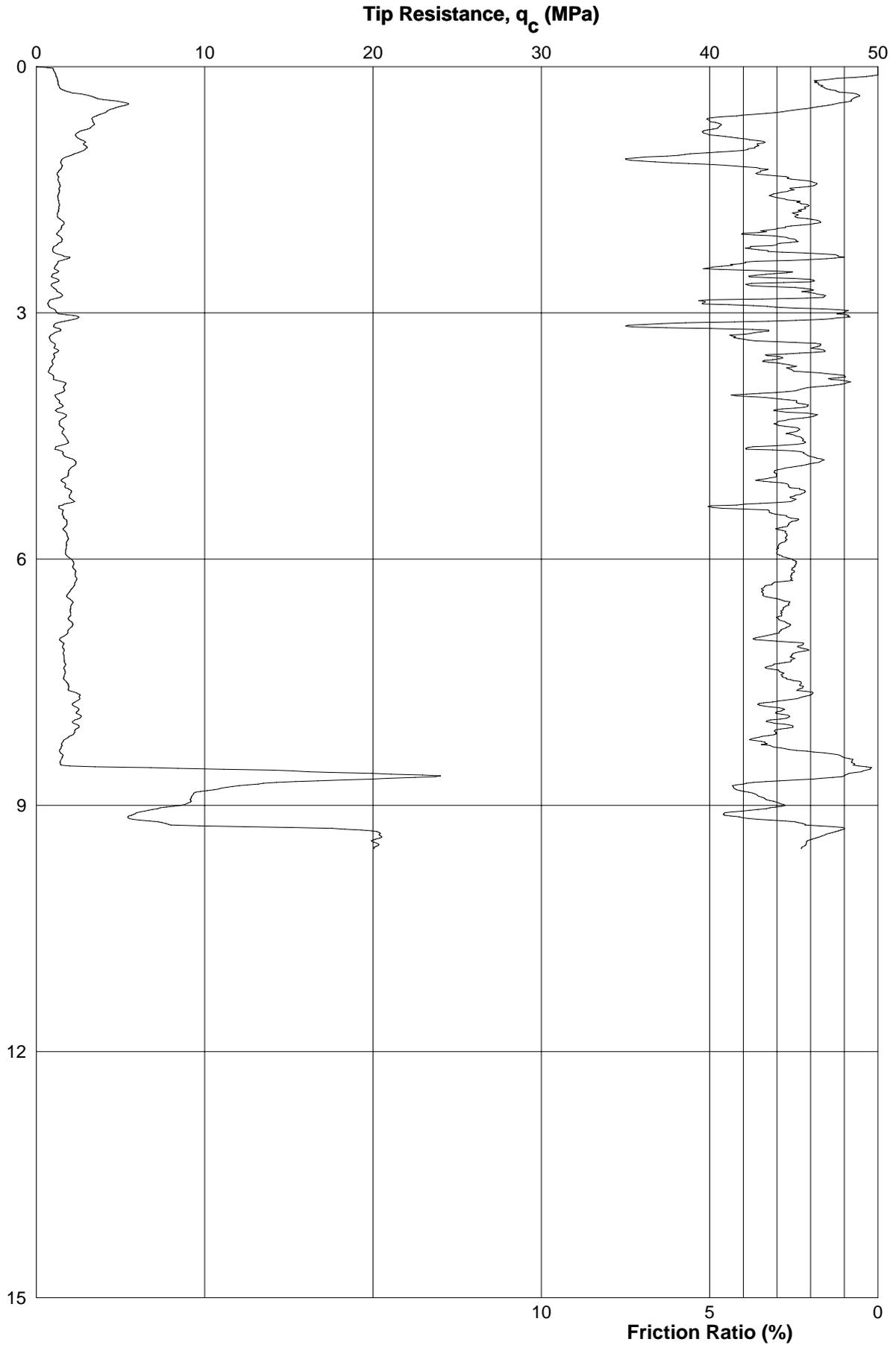
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STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 203

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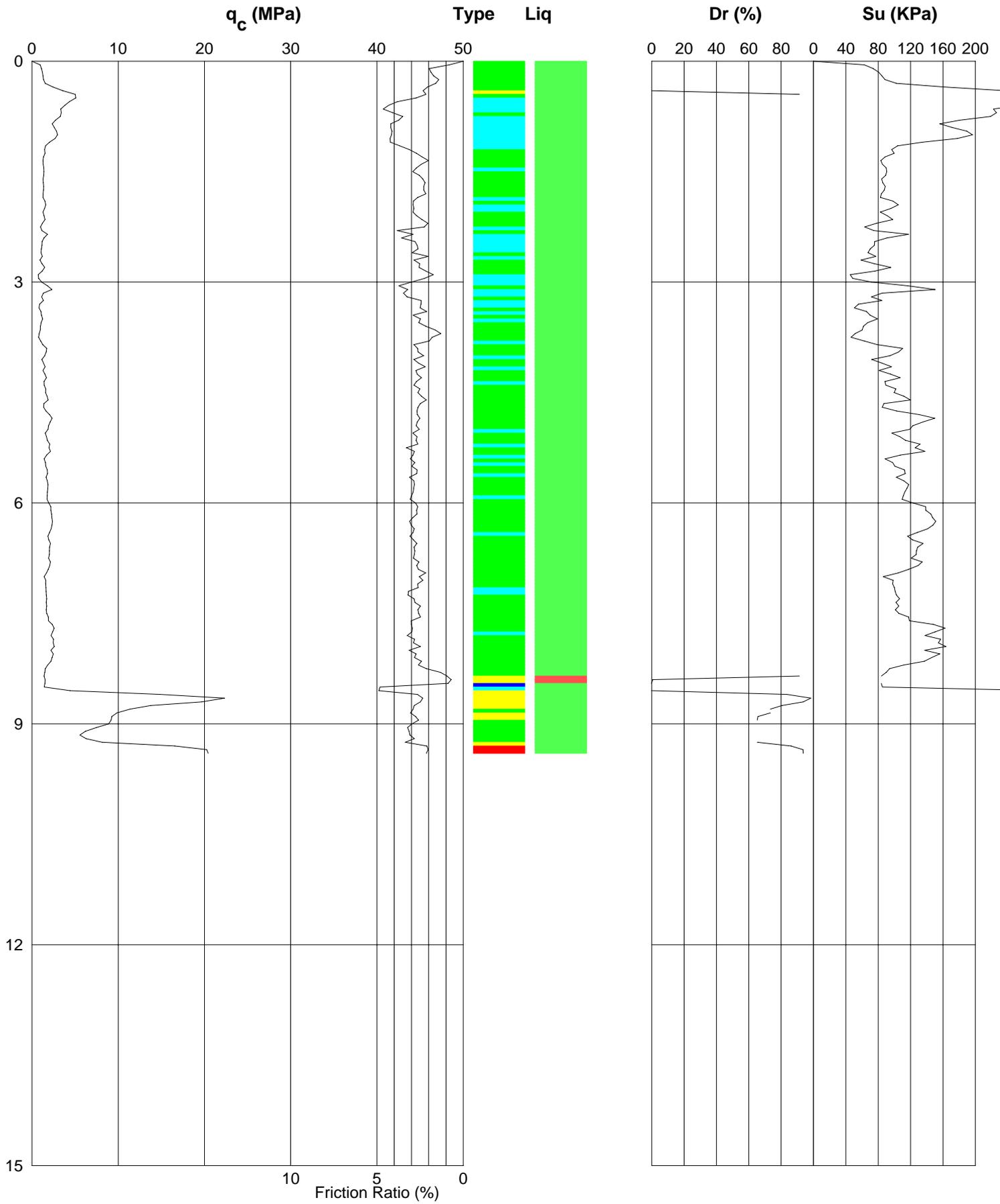
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Job No: 4934

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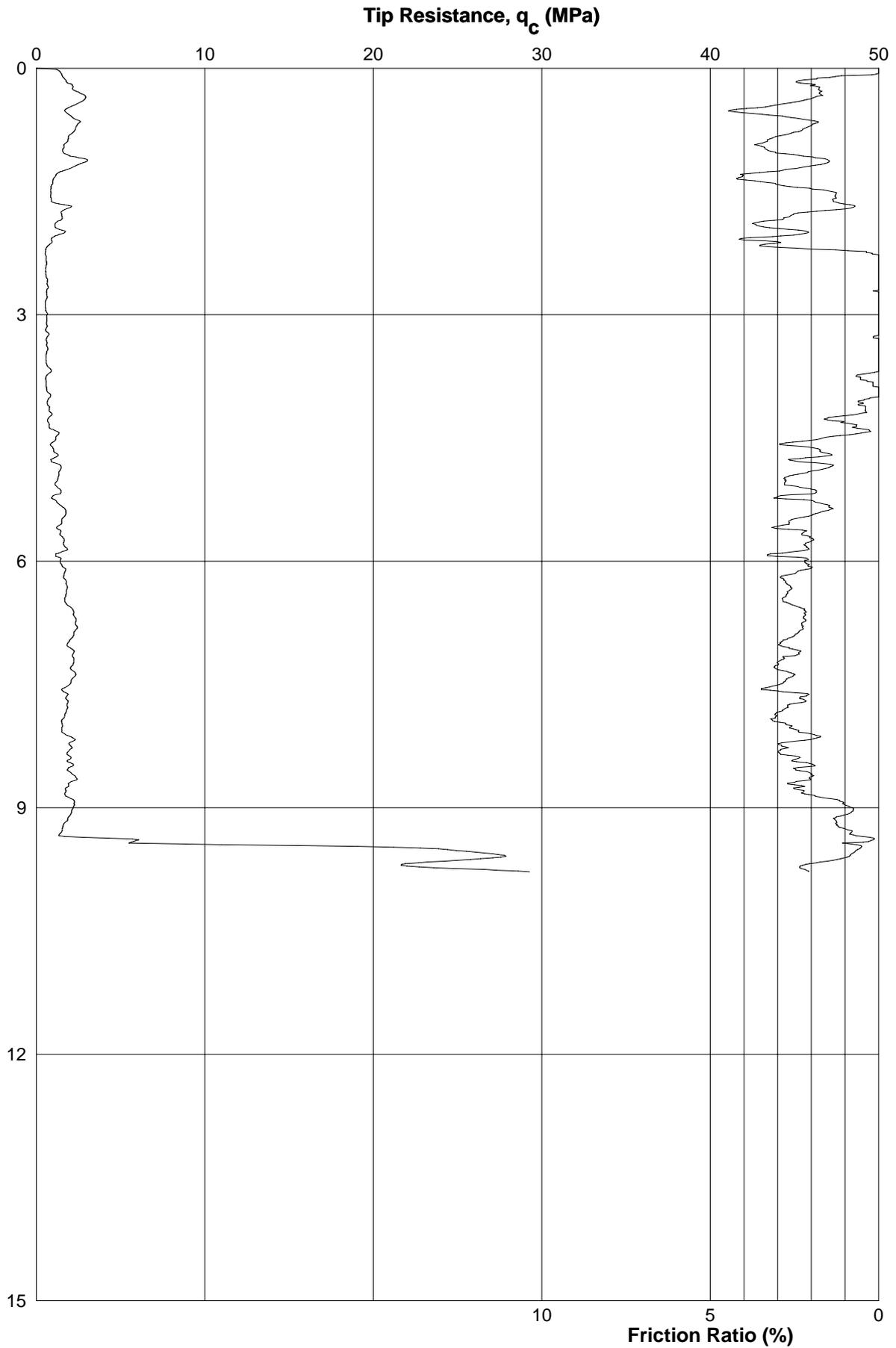
Location: Jacks Point, Queenstown

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Job No: 4934

CPT No: 204

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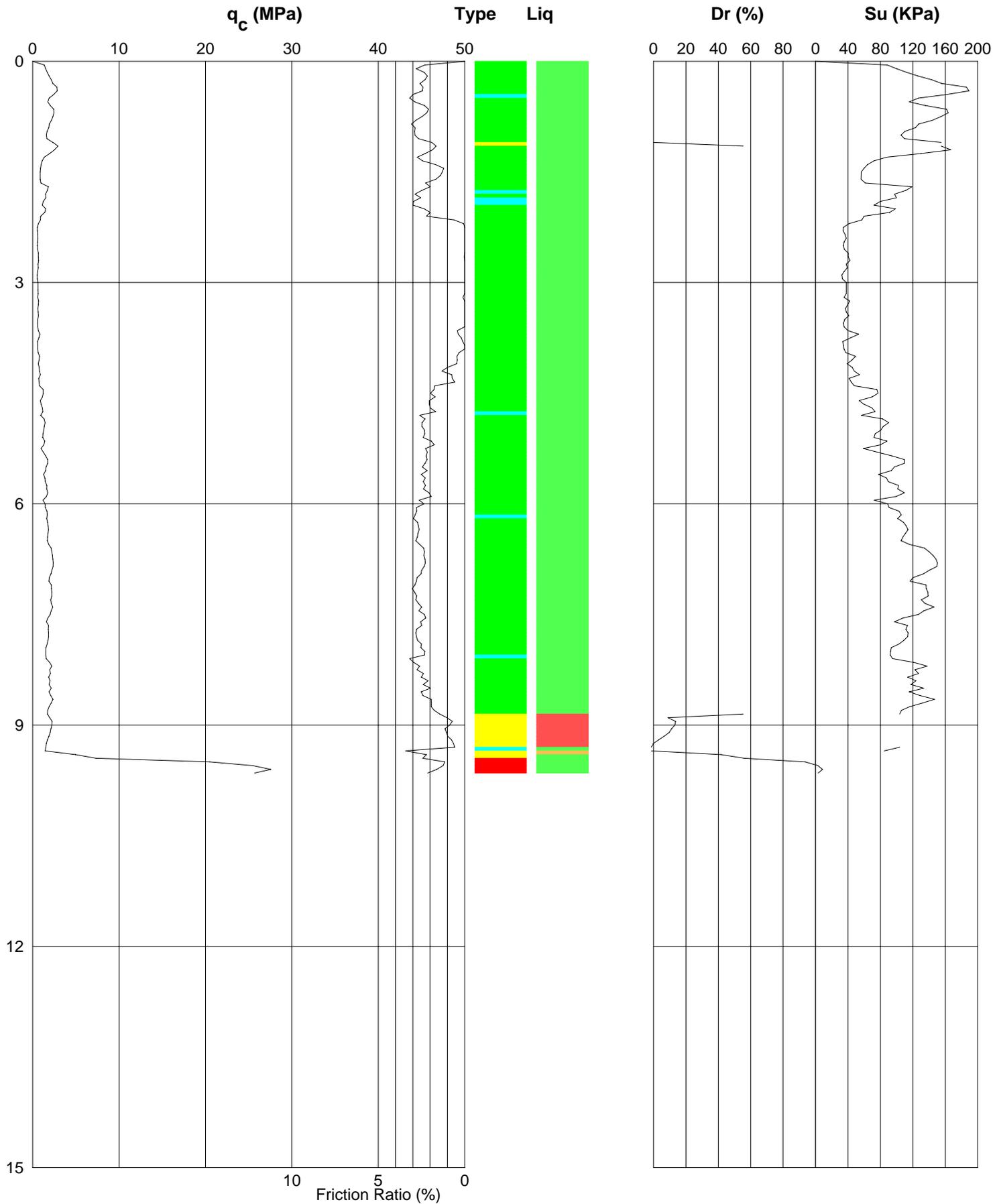
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Job No: 4934

CPT No: 204

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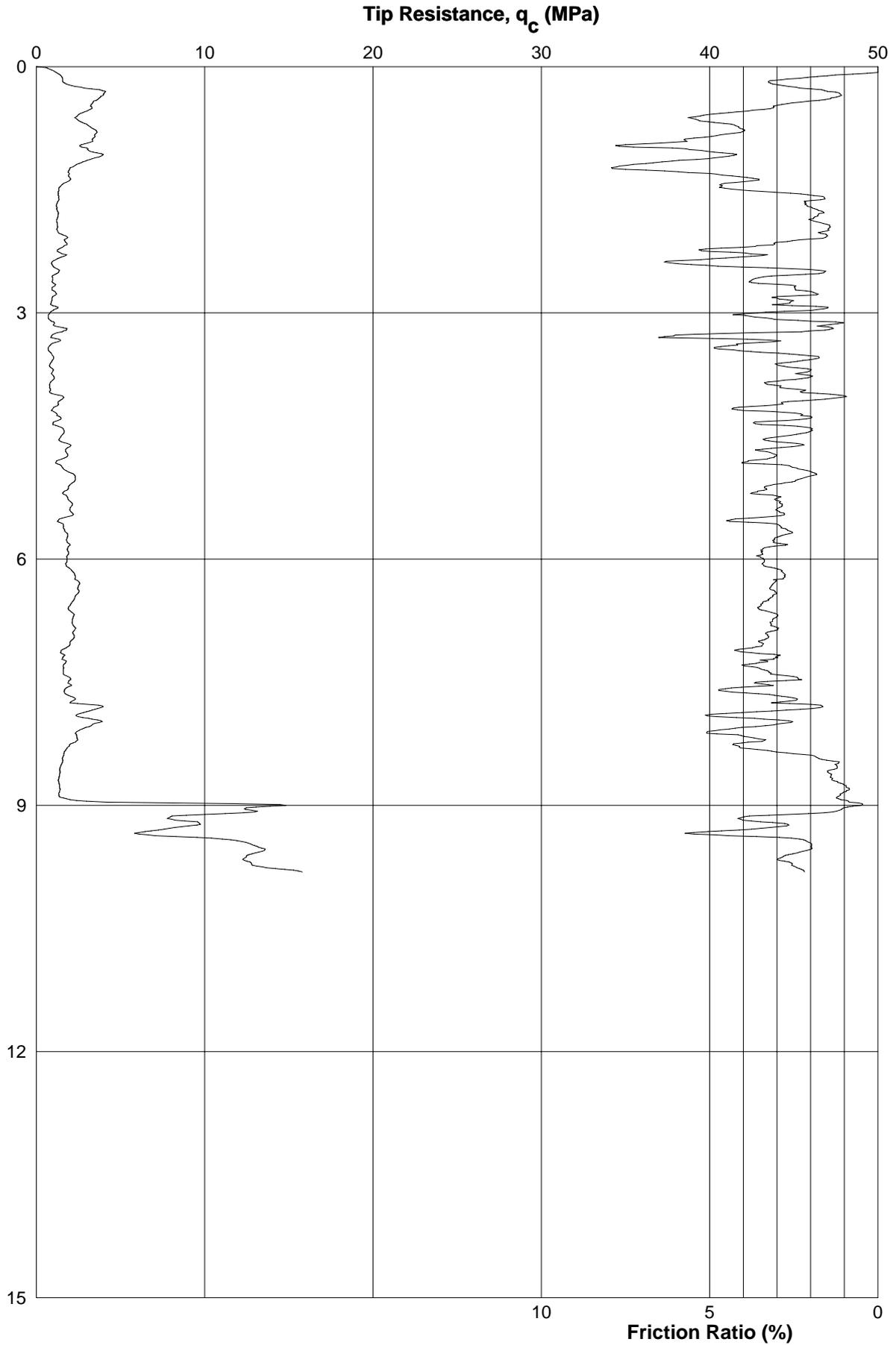
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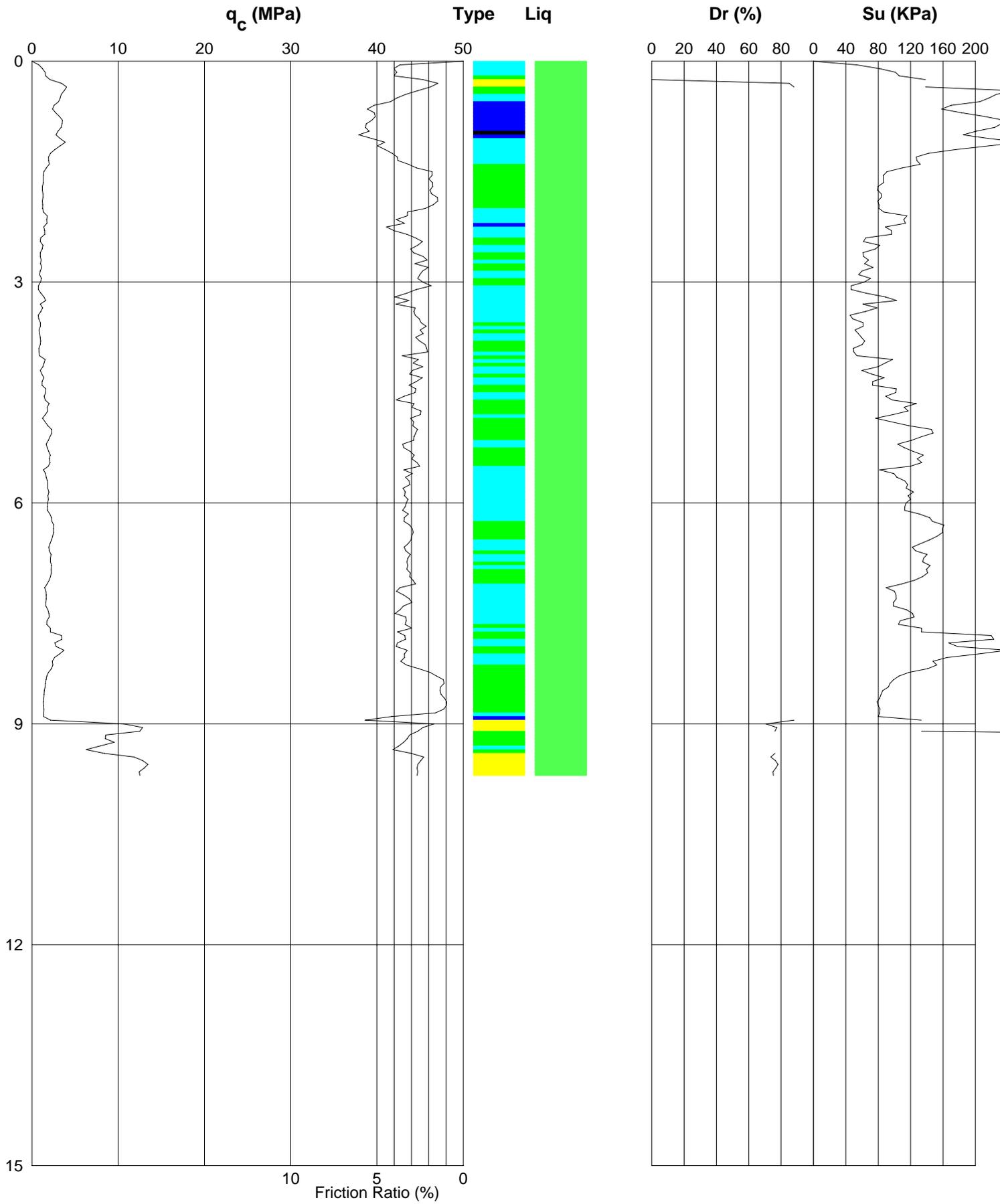
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Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

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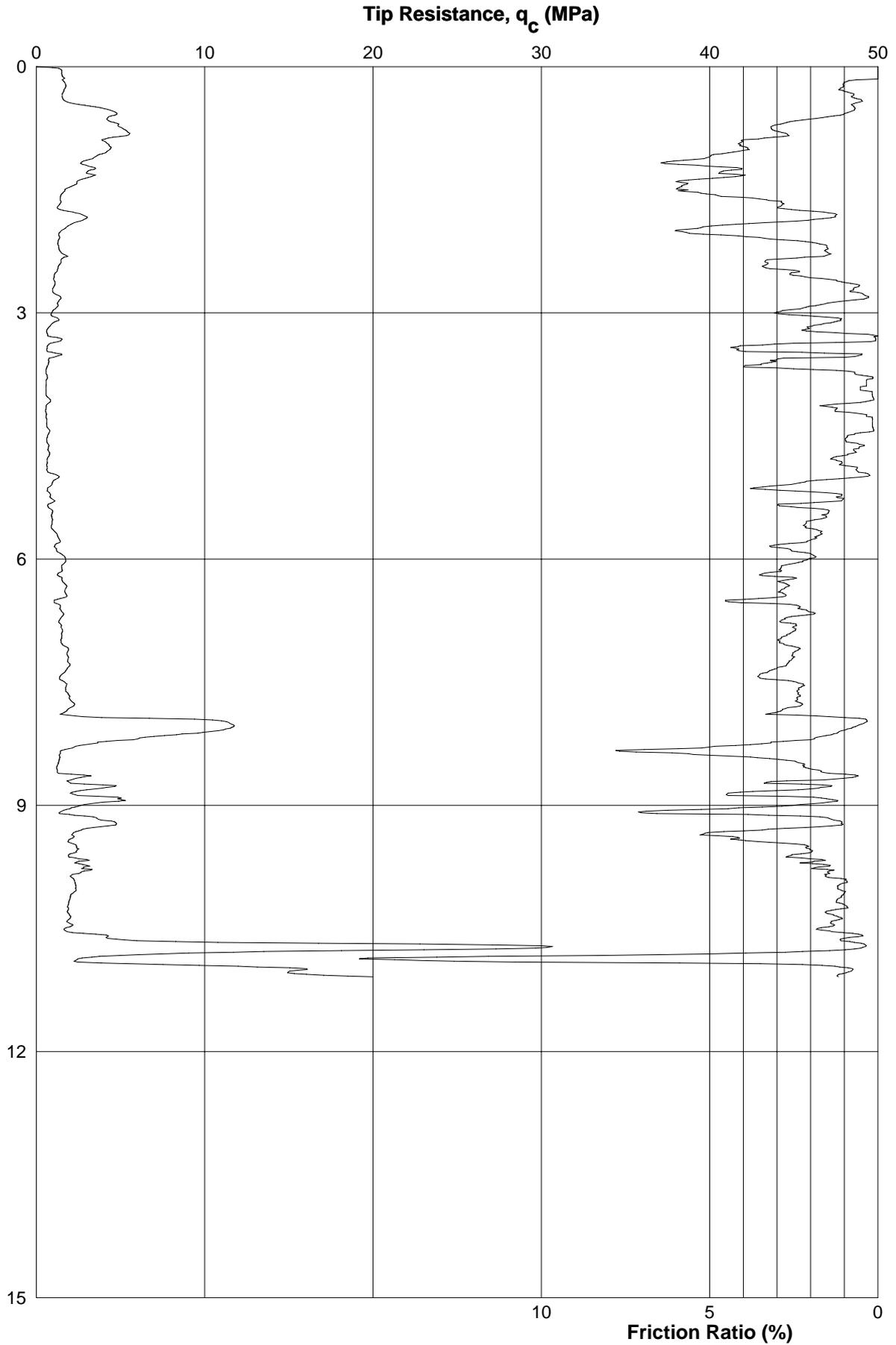
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Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

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Job No: 4934

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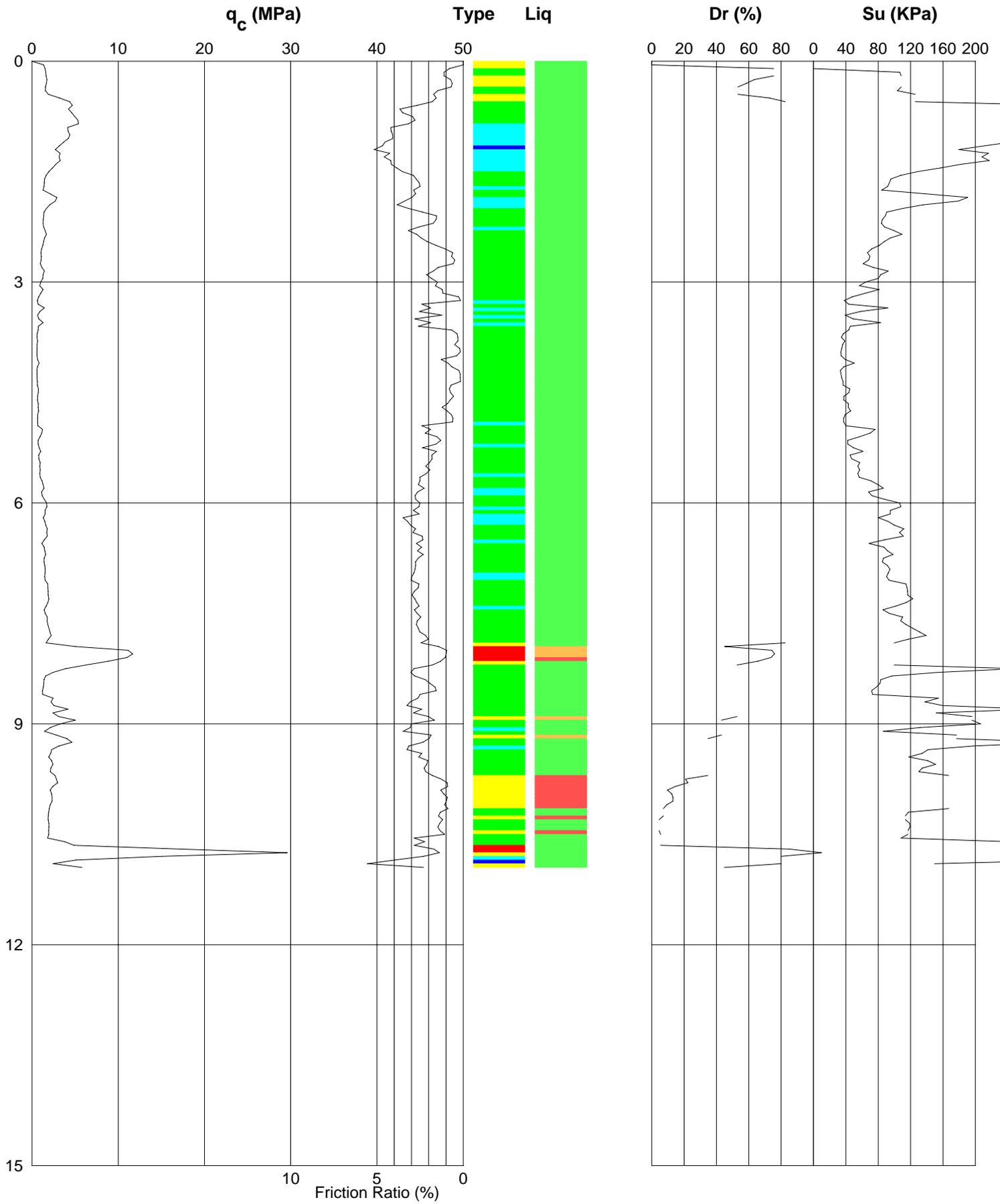
Location: Jacks Point, Queenstown

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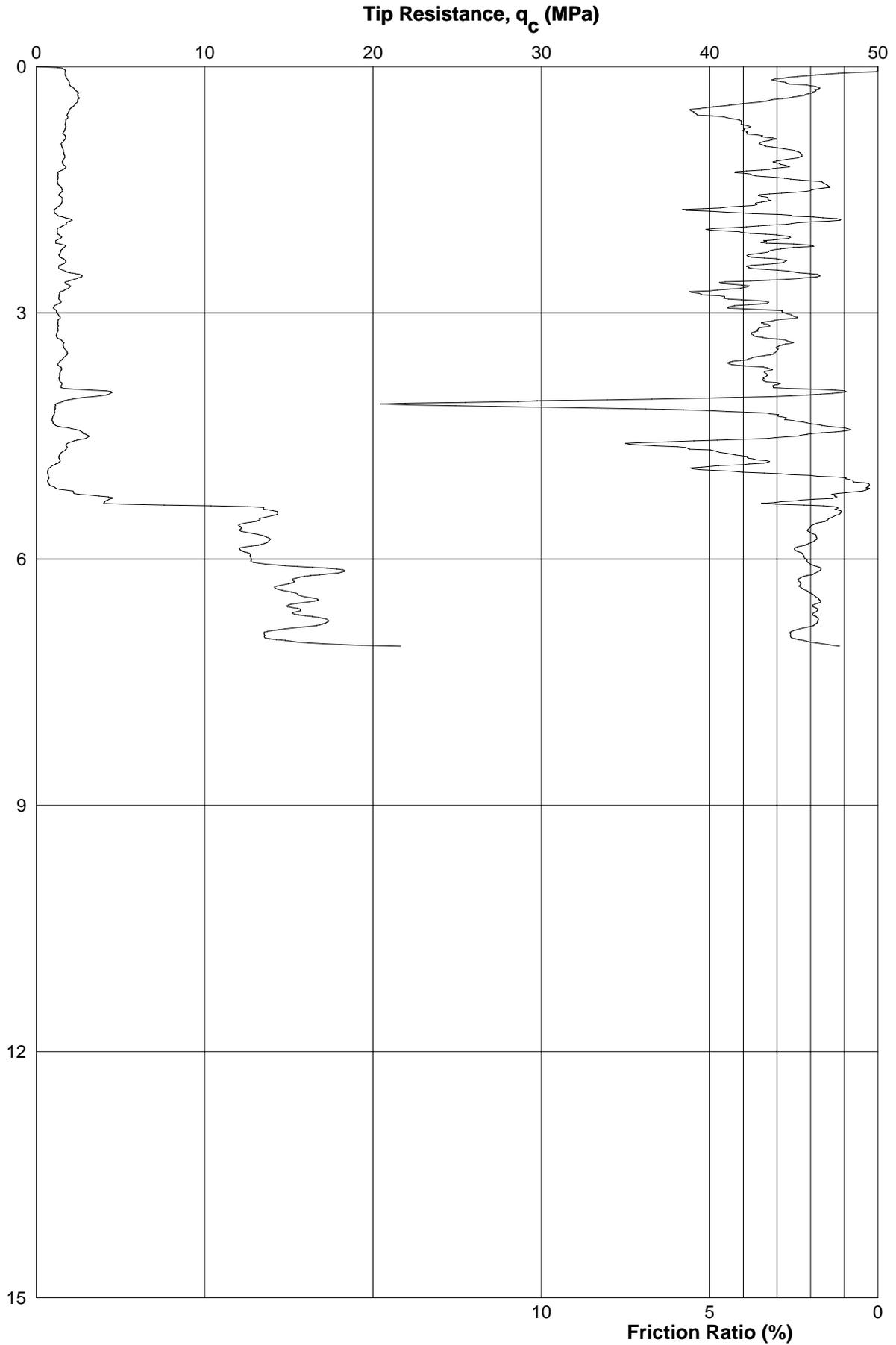
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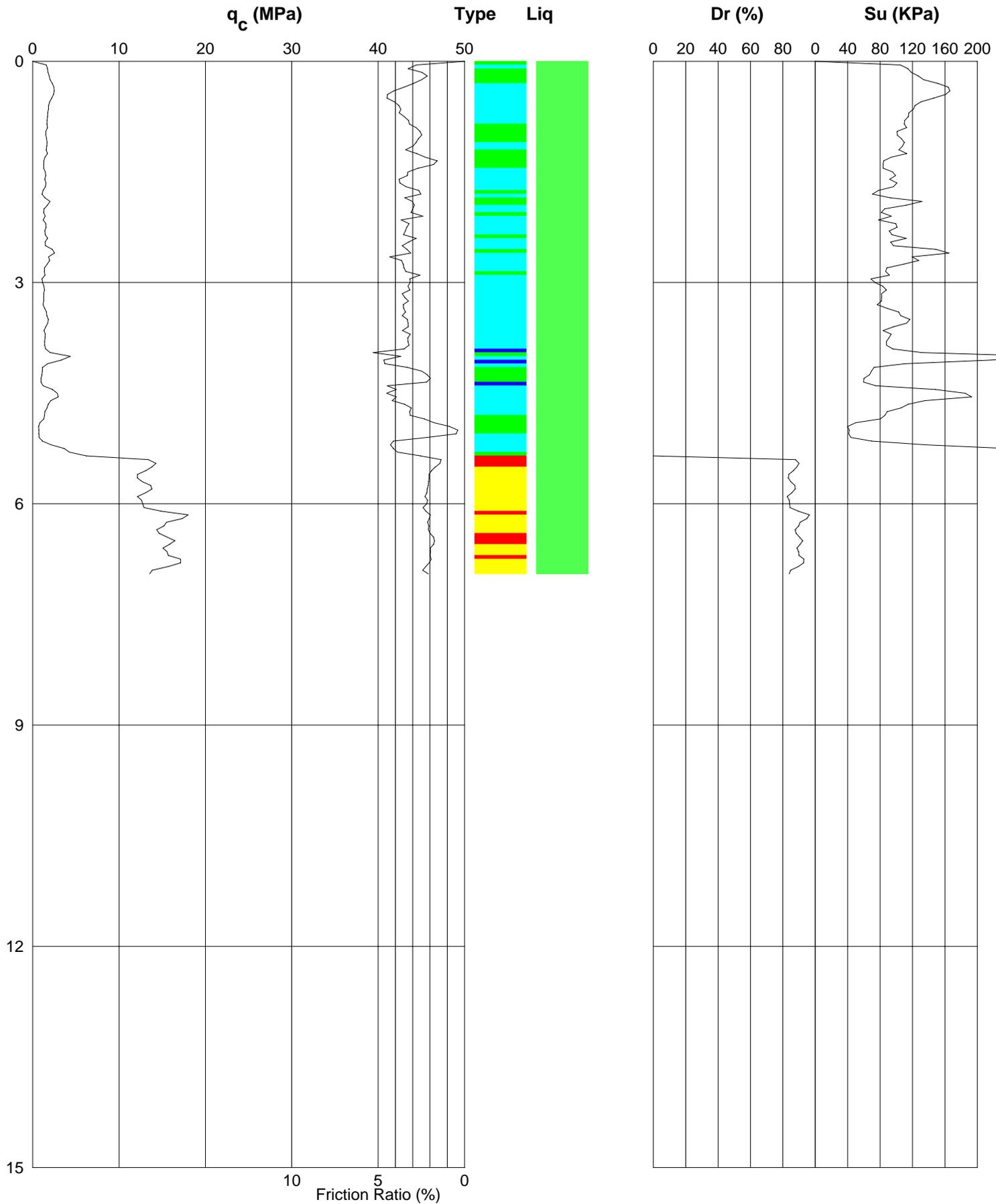
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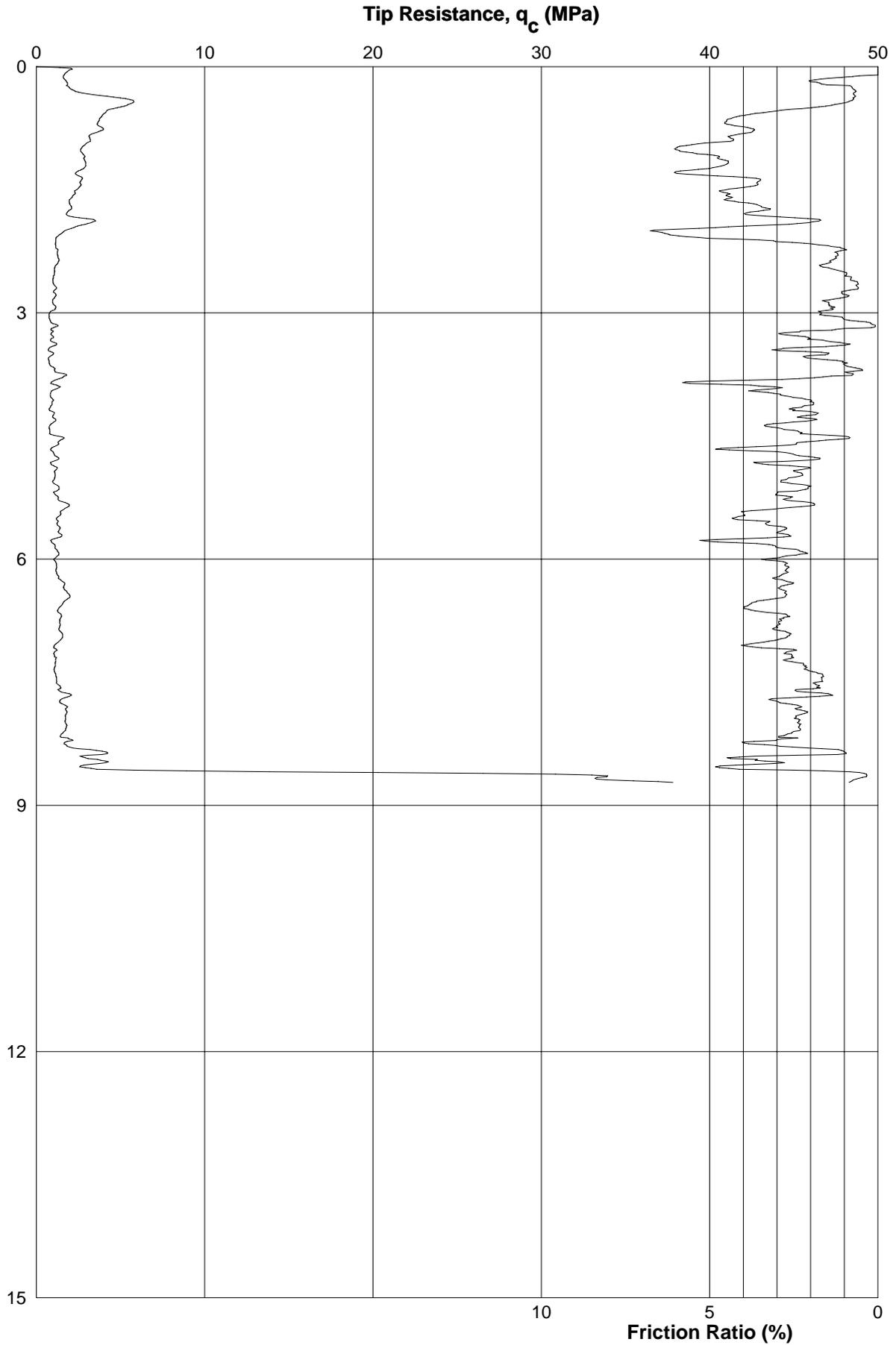
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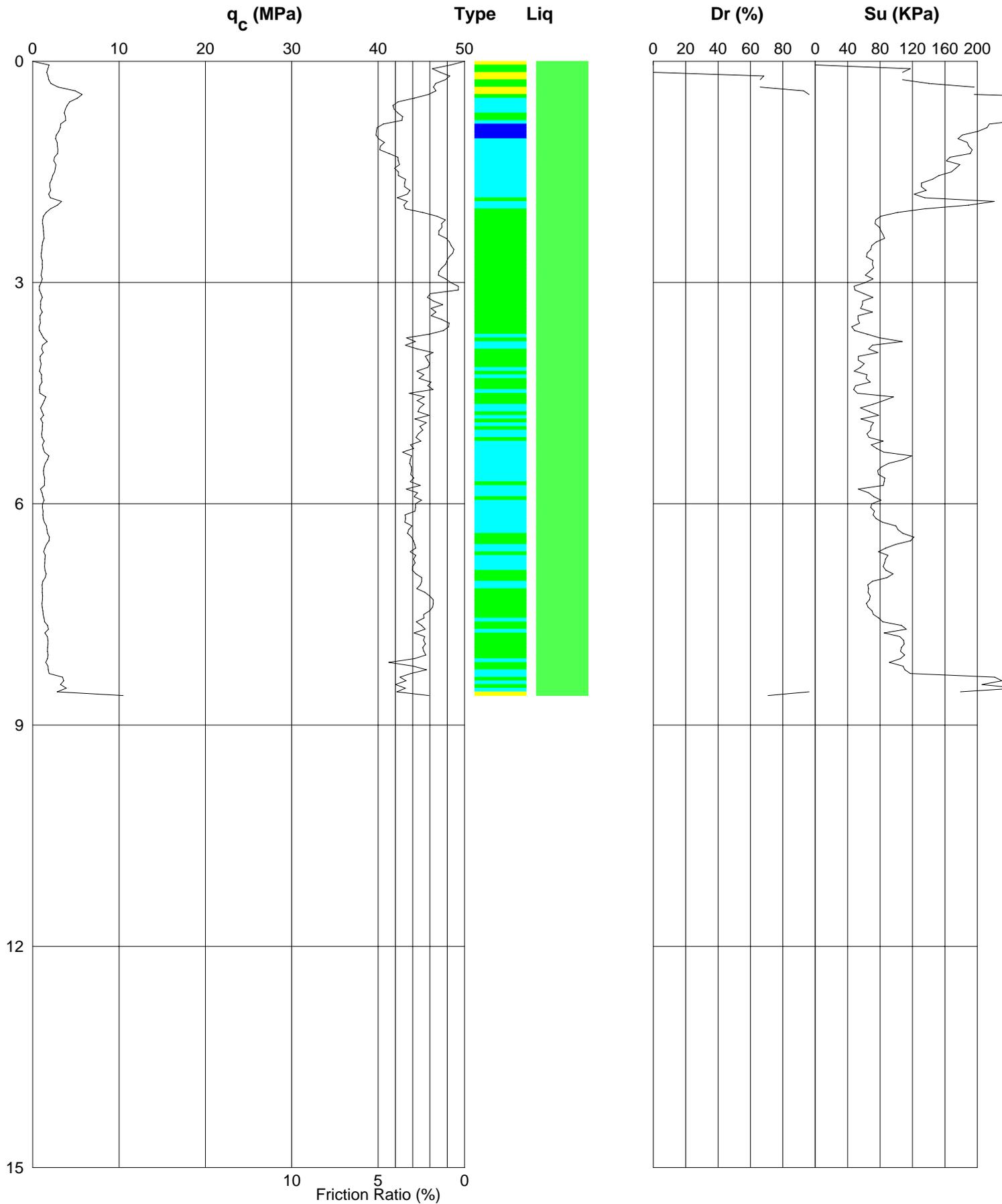
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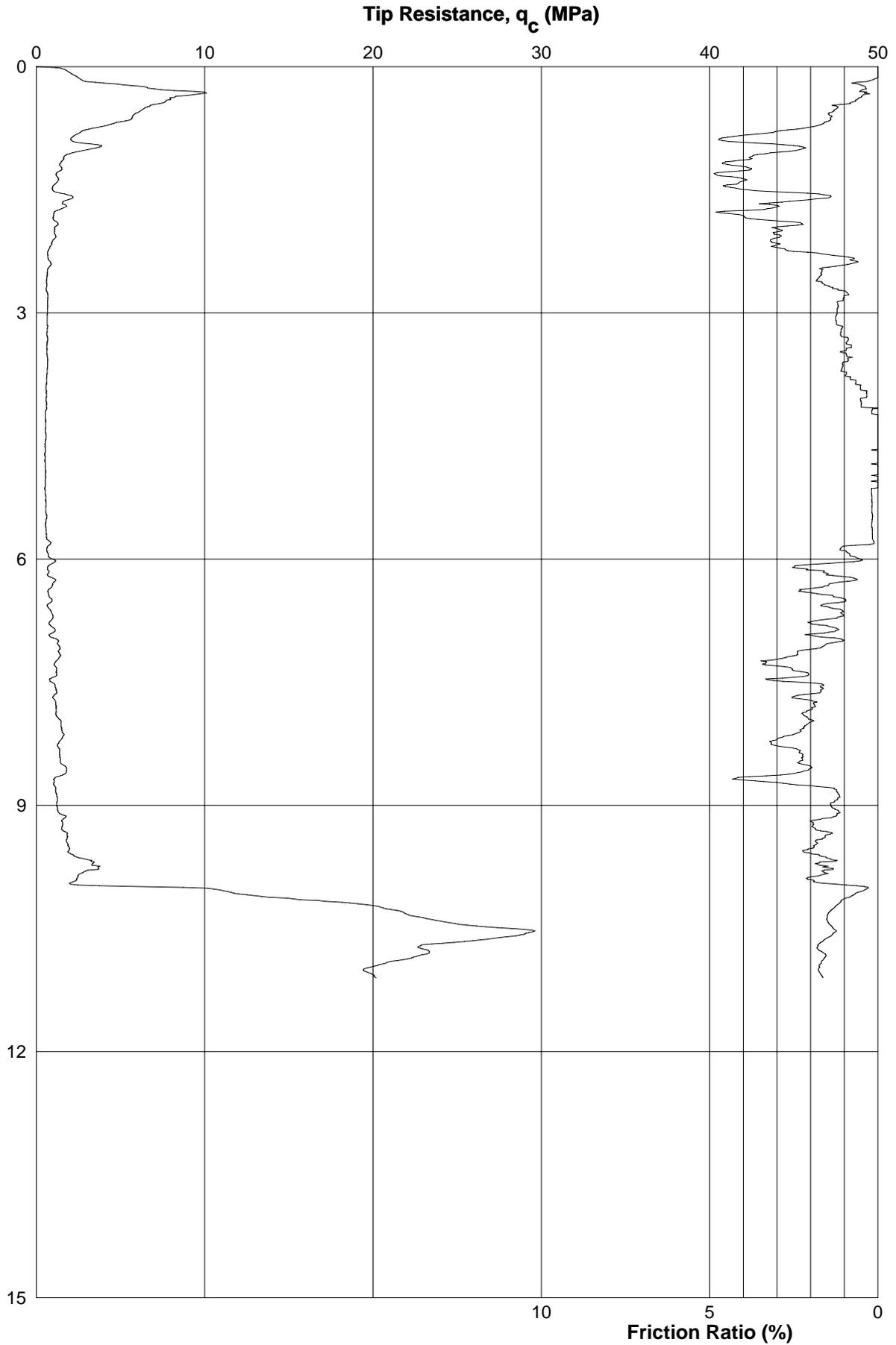
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STANDARD CONE PENETROMETER TEST (CPT) REPORT



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CPT No: 209

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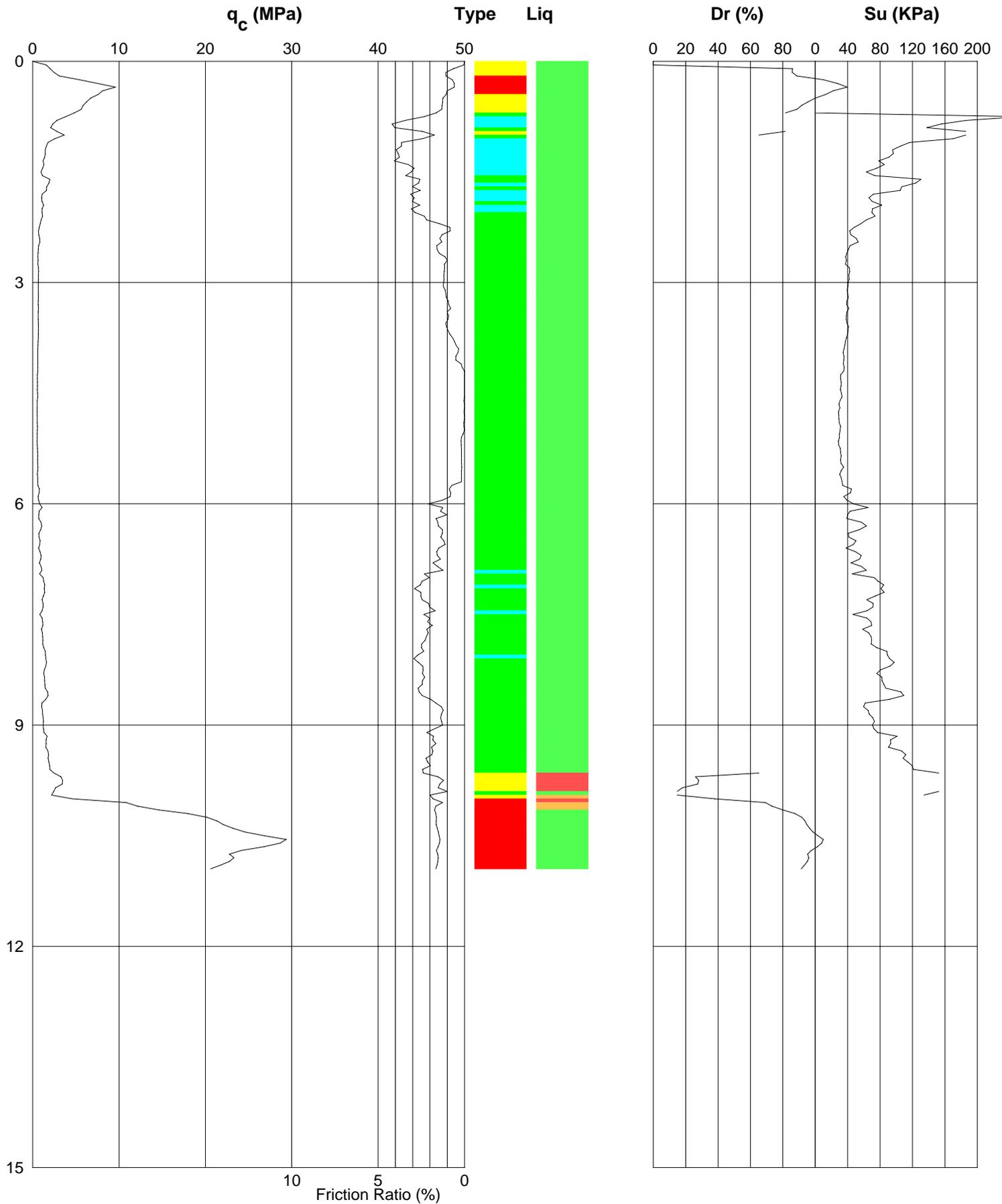
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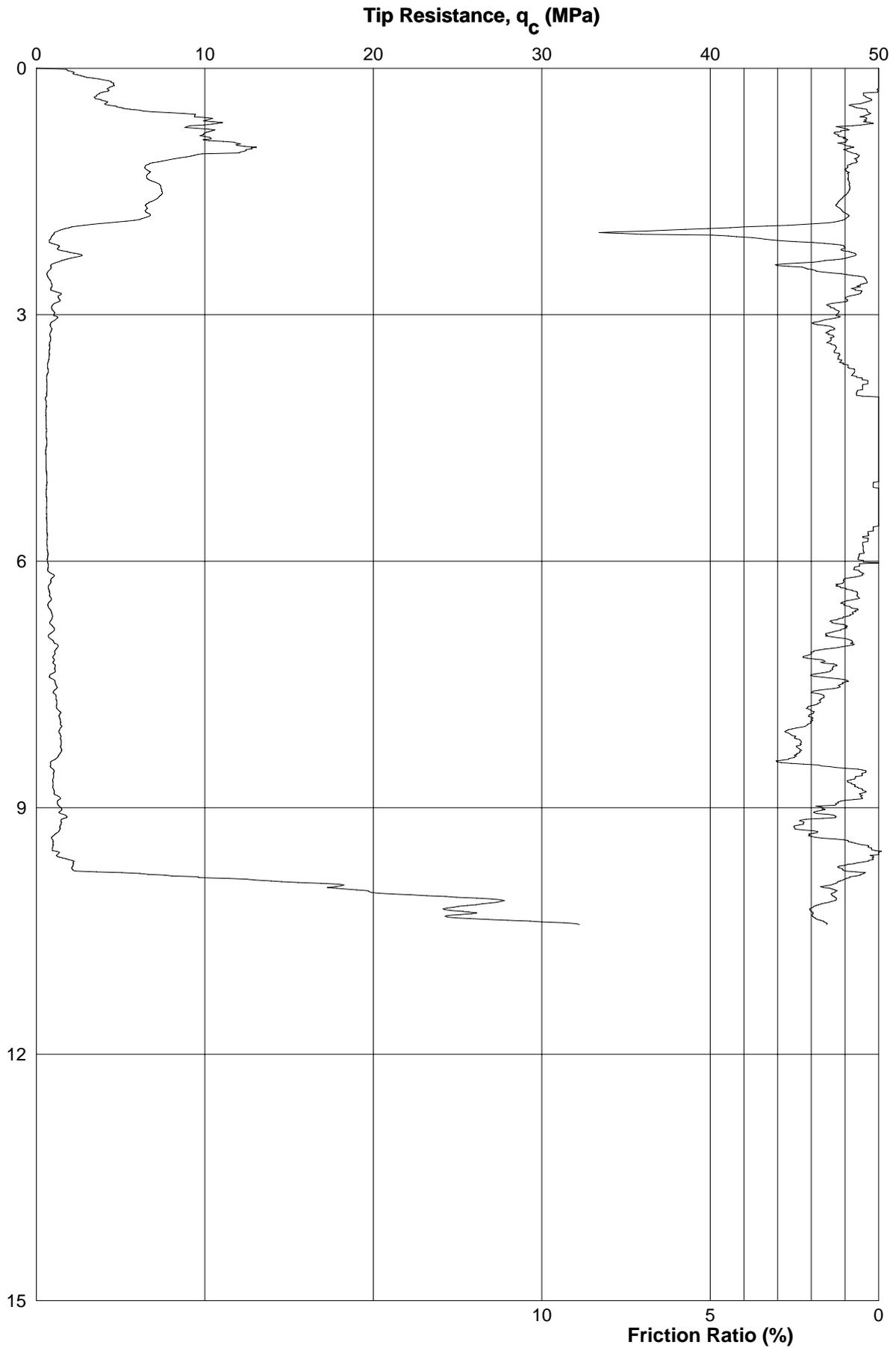
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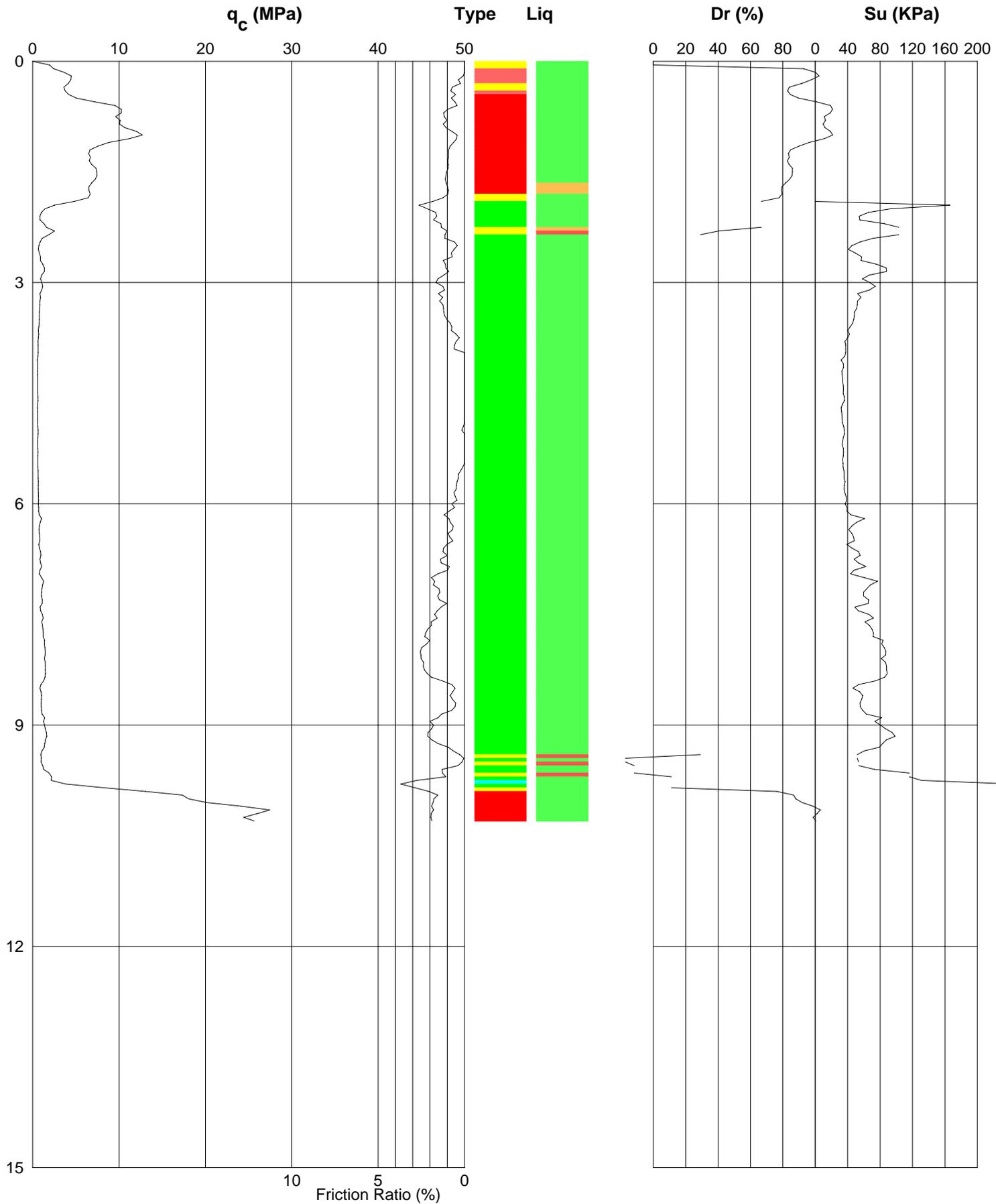
Location: Jacks Point, Queenstown

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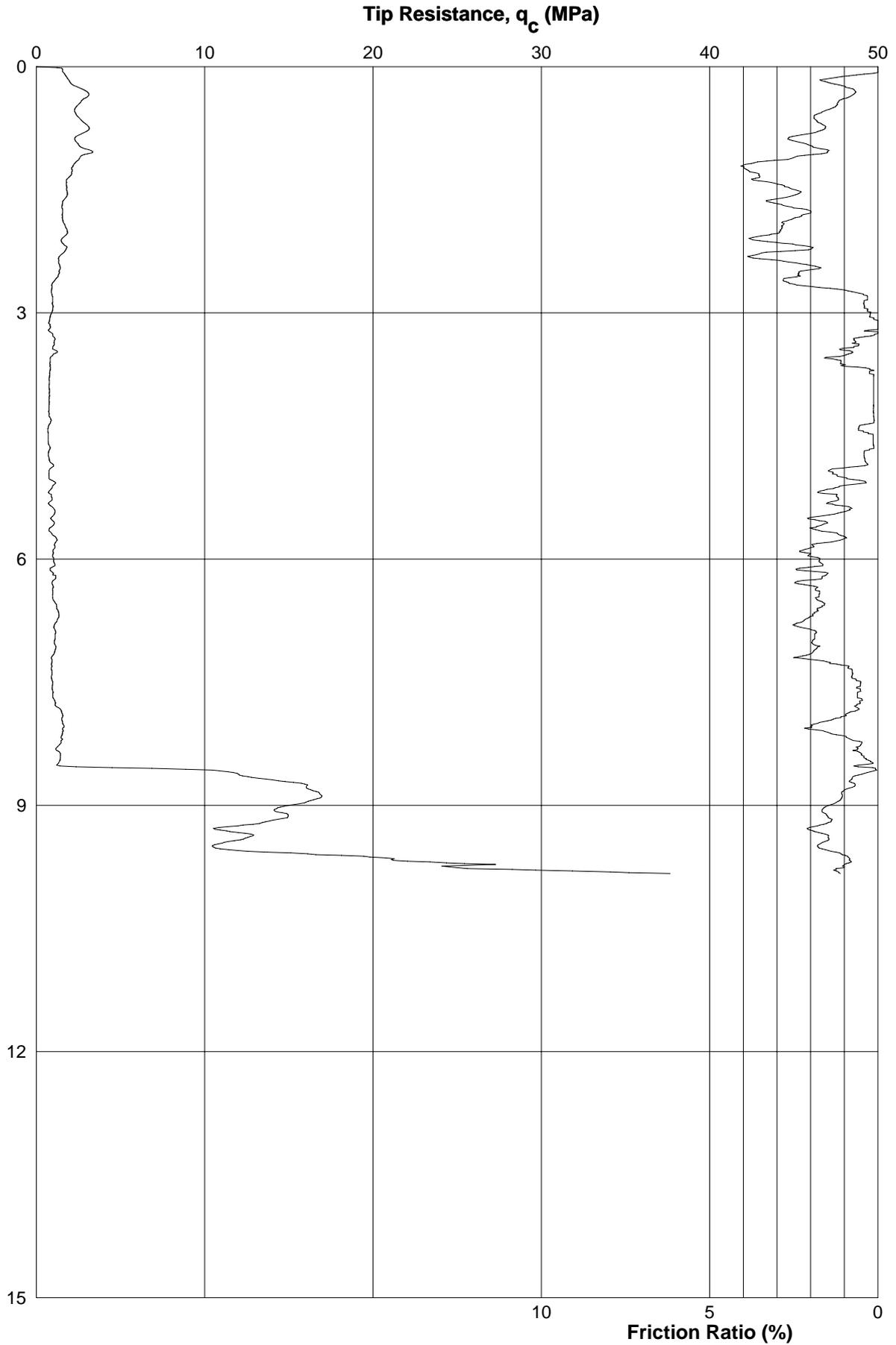
Location: Jacks Point, Queenstown

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Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



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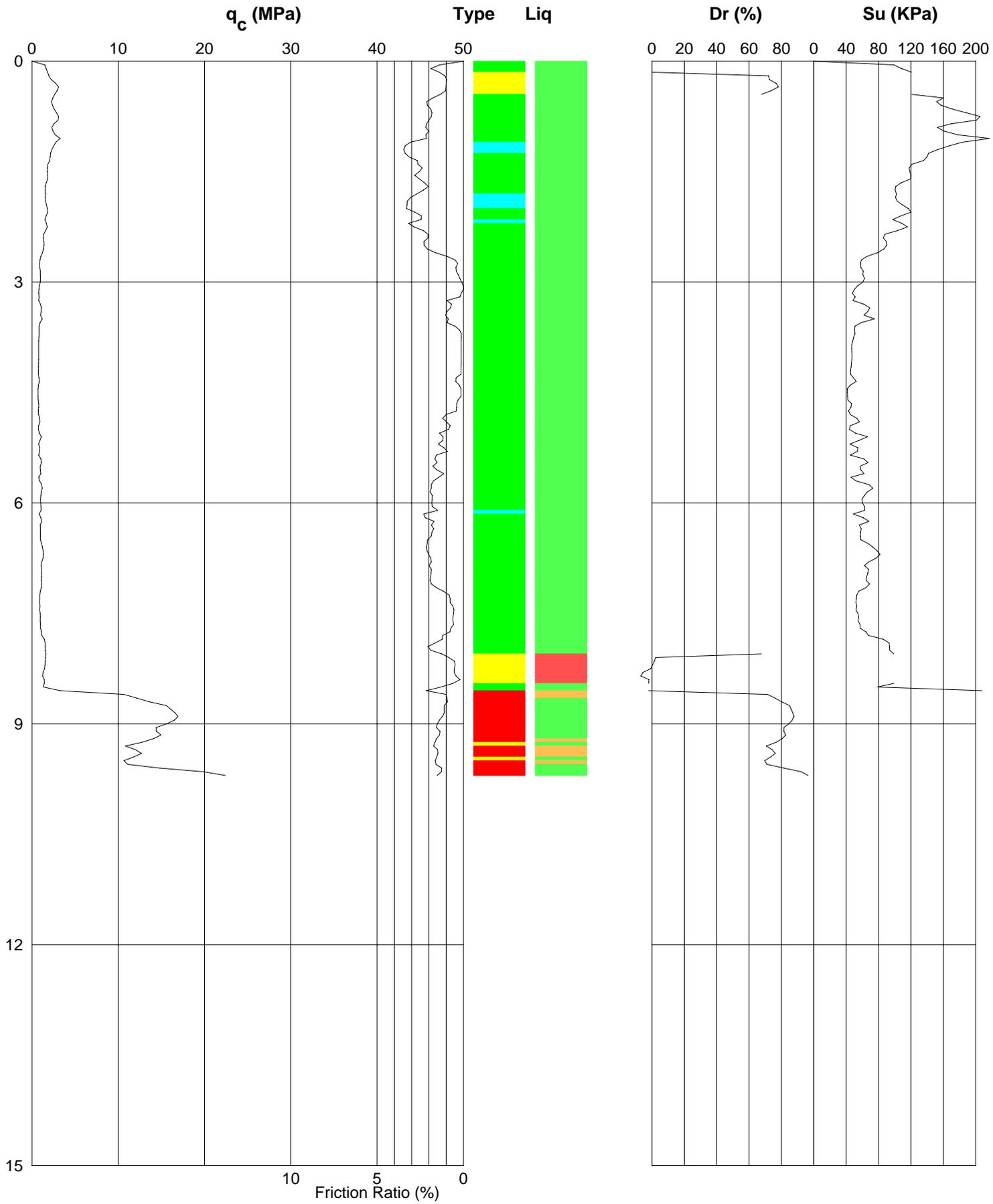
Location: Jacks Point, Queenstown

Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

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Job No: 4934

CPT No: 211

Project: Tonkin & Taylor Ltd

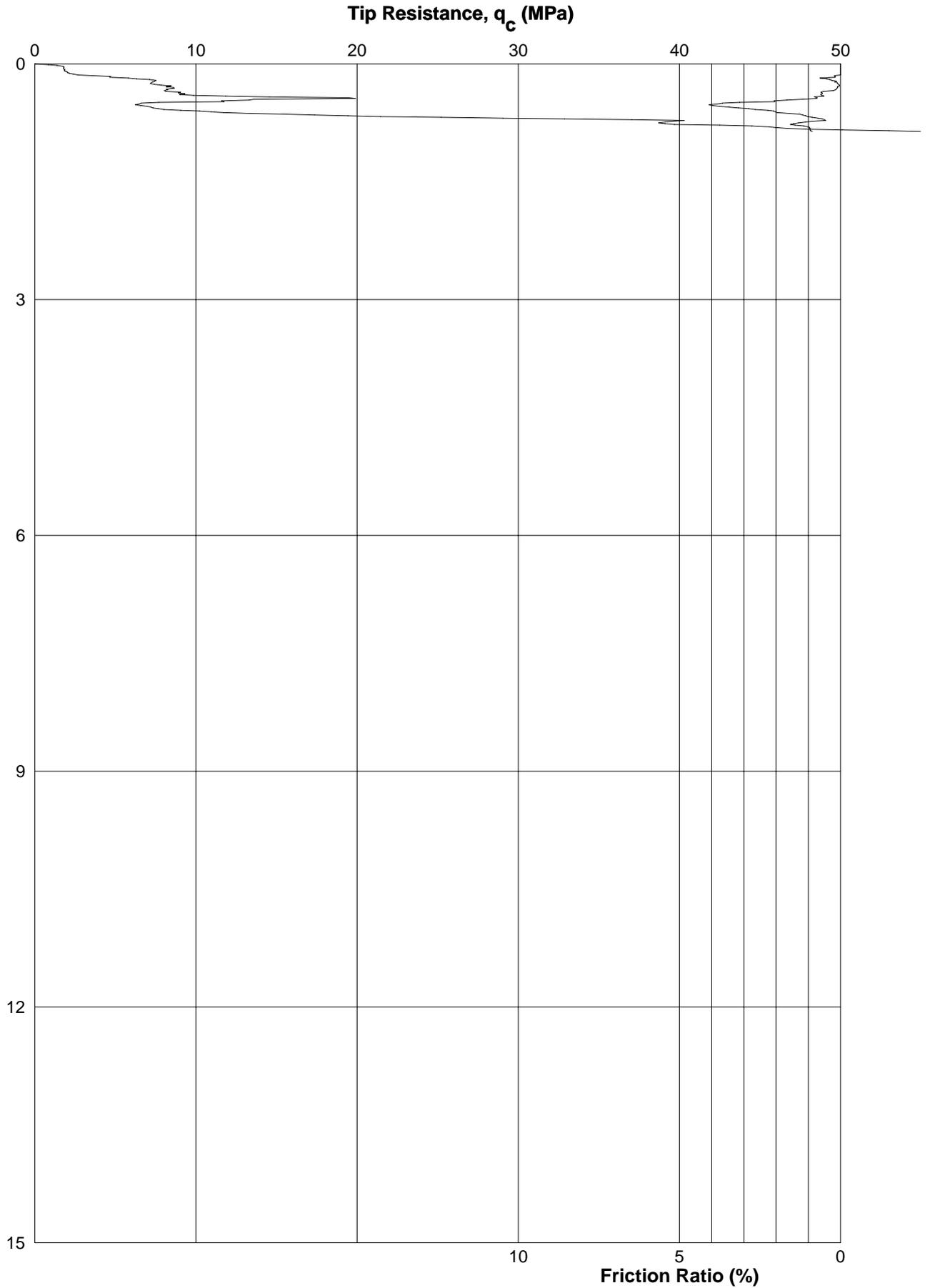
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Operator: J.Harvey

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CPT No: 212

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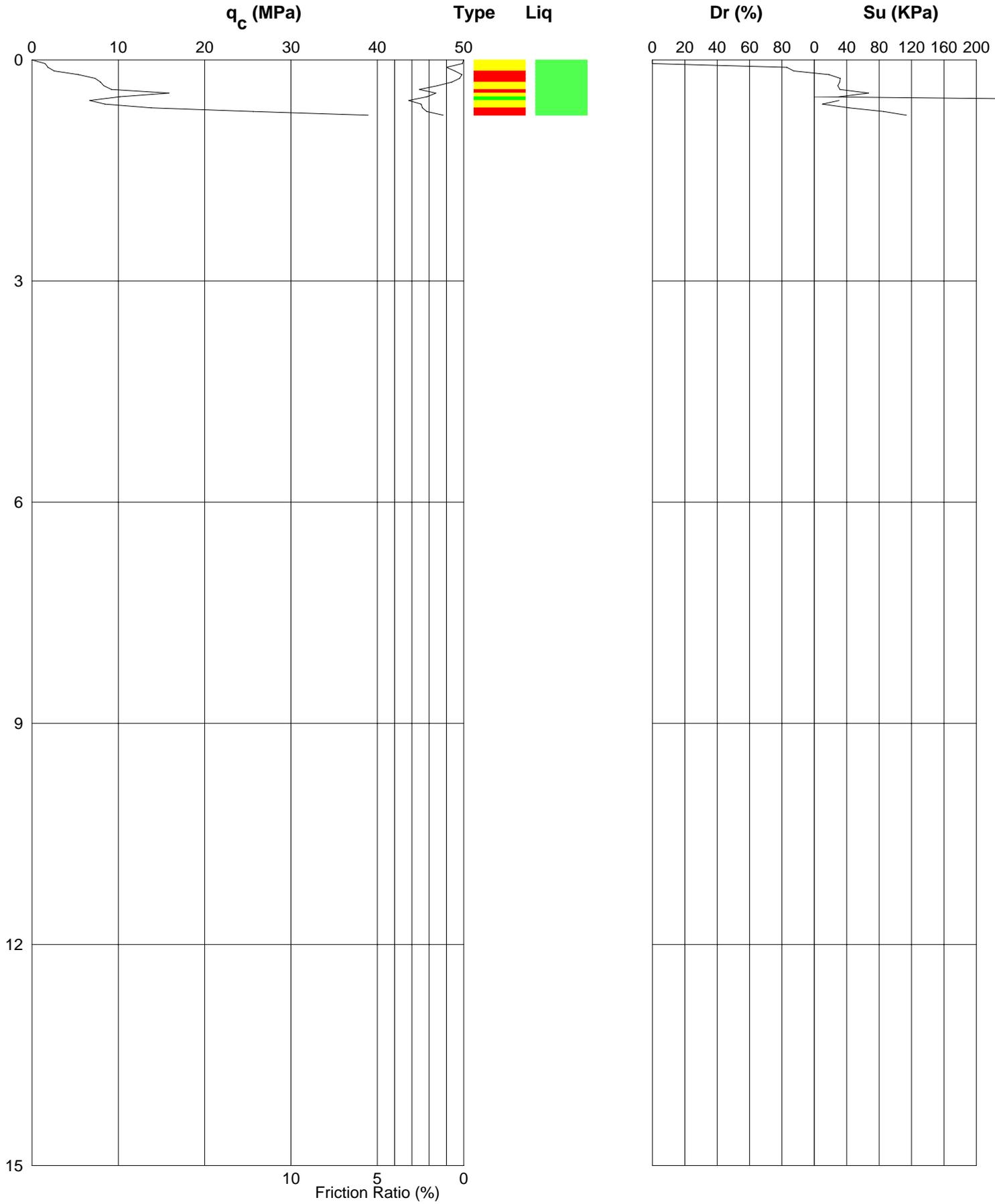
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Remark: Effective Refusal

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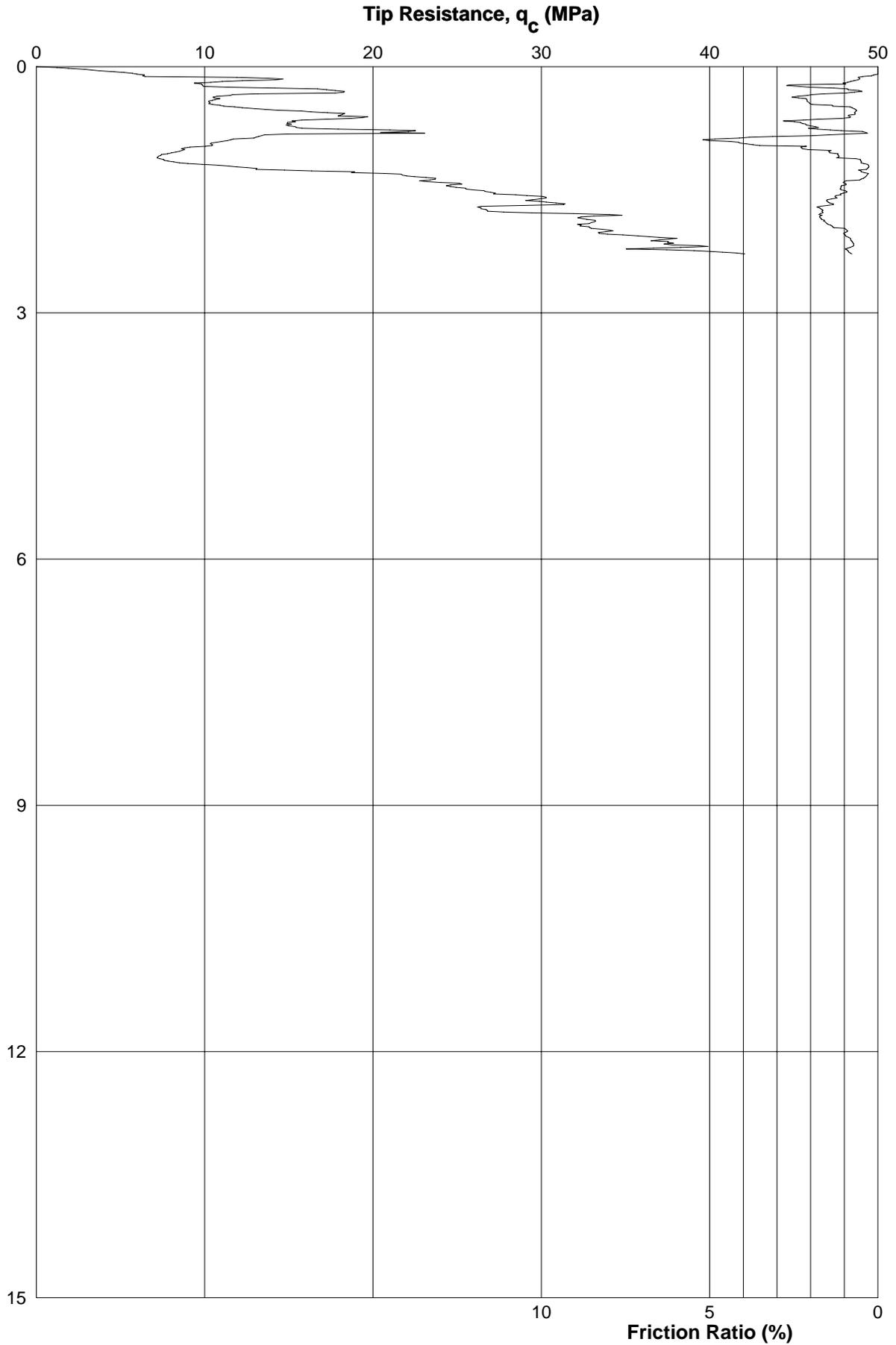
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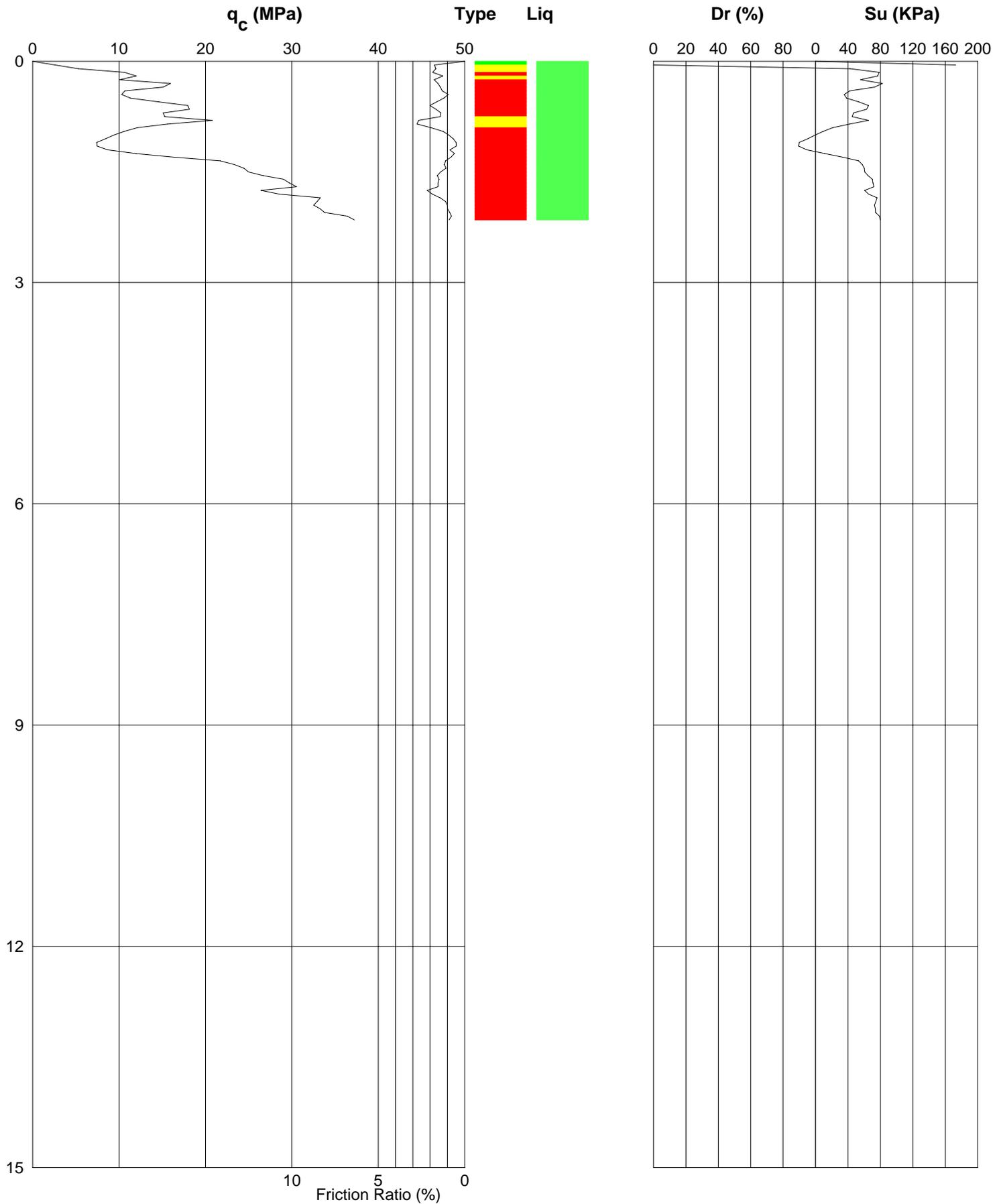
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CPT No: 213

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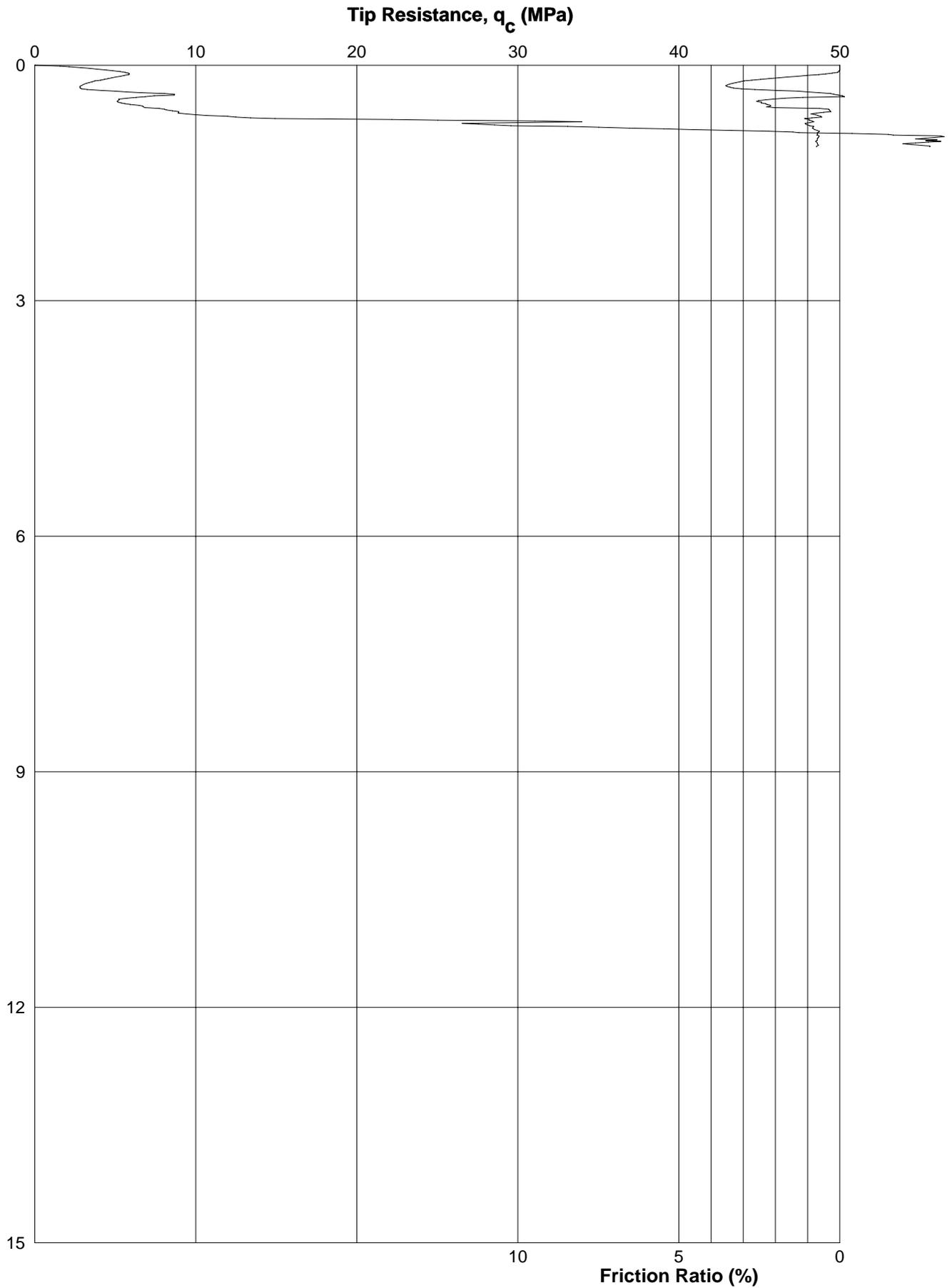
Location: Jacks Point, Queenstown

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Job No: 4934

CPT No: 214

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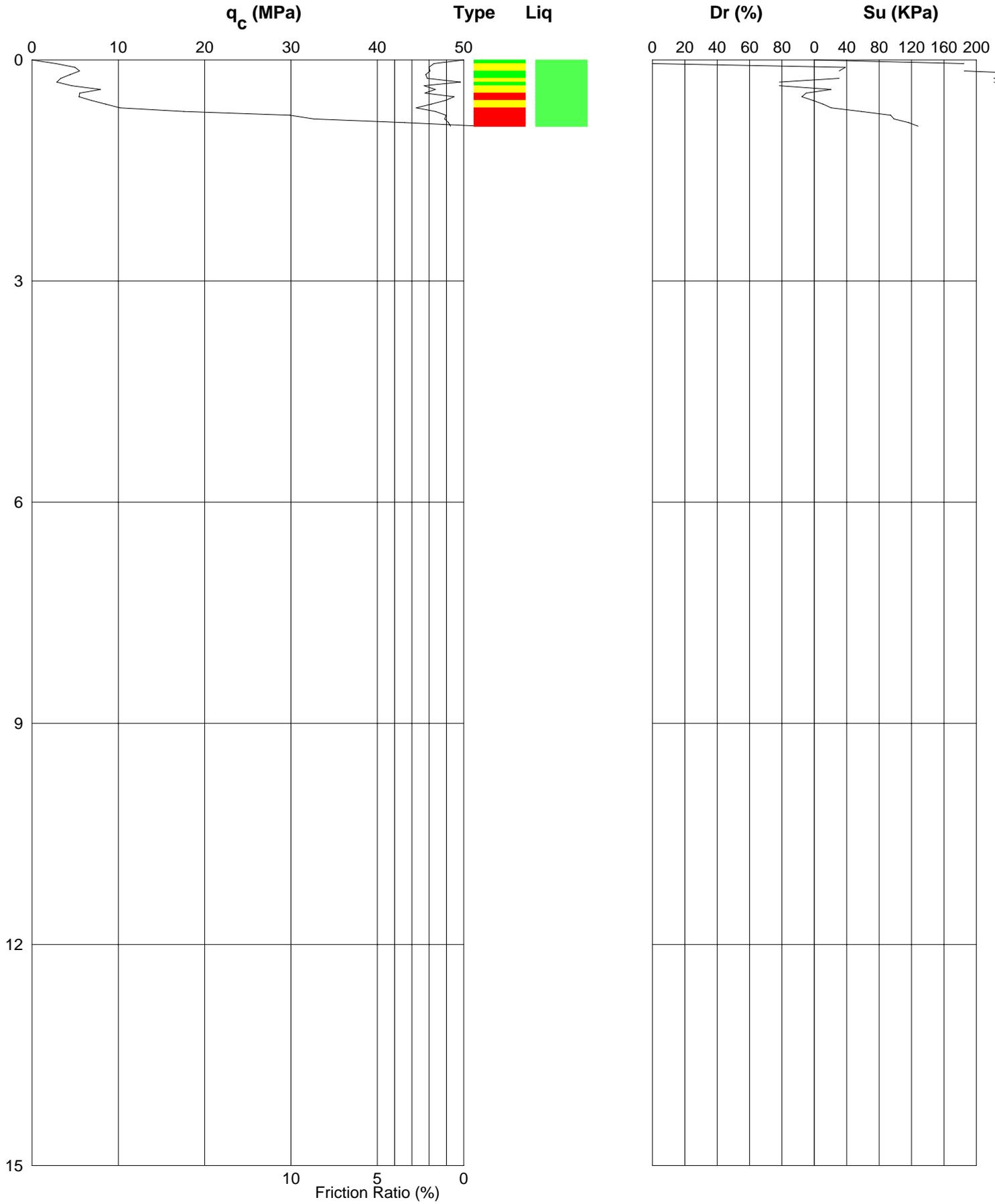
Location: Jacks Point, Queenstown

Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

CPT No: 214

Project: Tonkin & Taylor Ltd

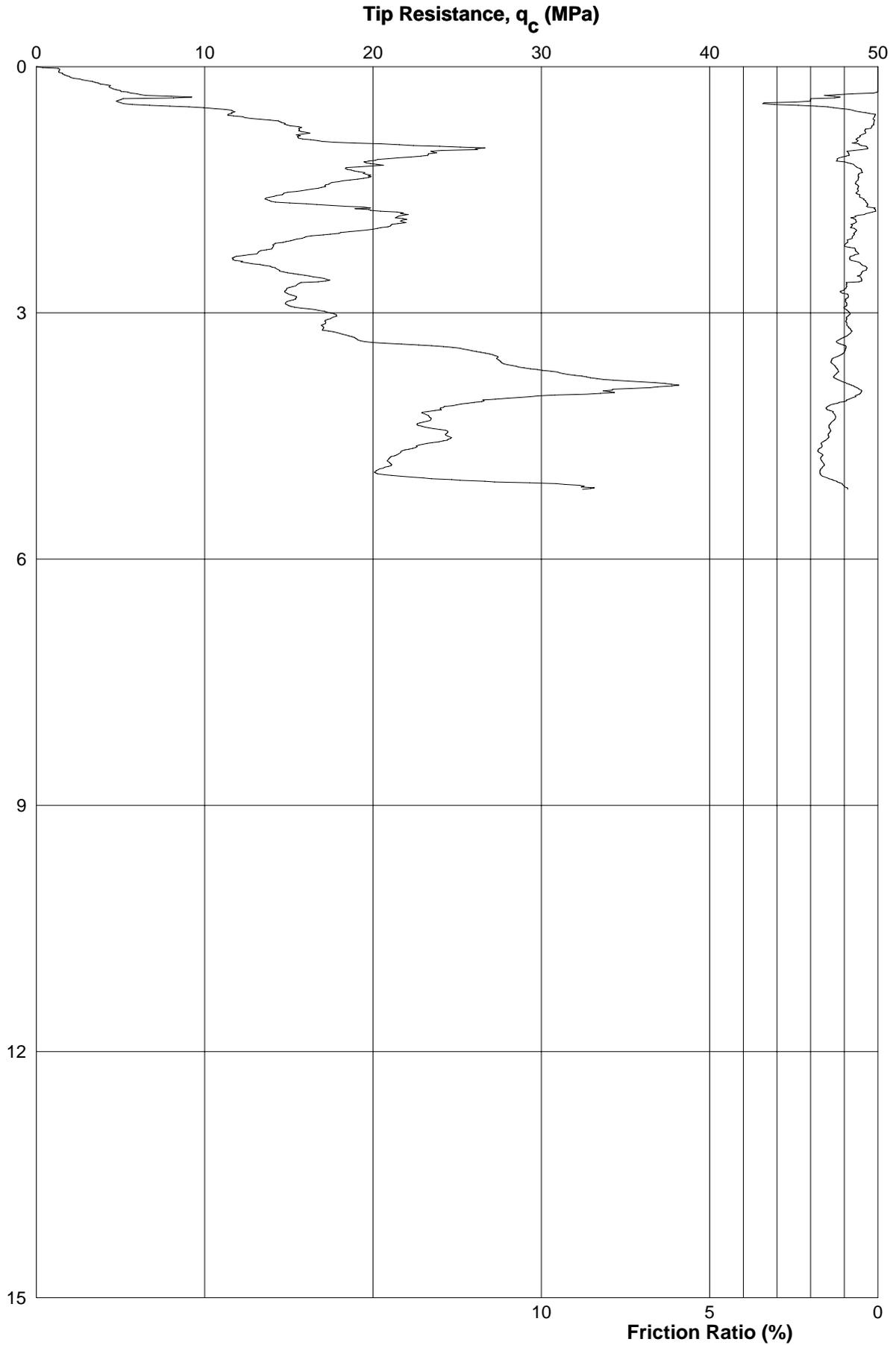
Location: Jacks Point, Queenstown

Date: 27-9-07

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Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 215

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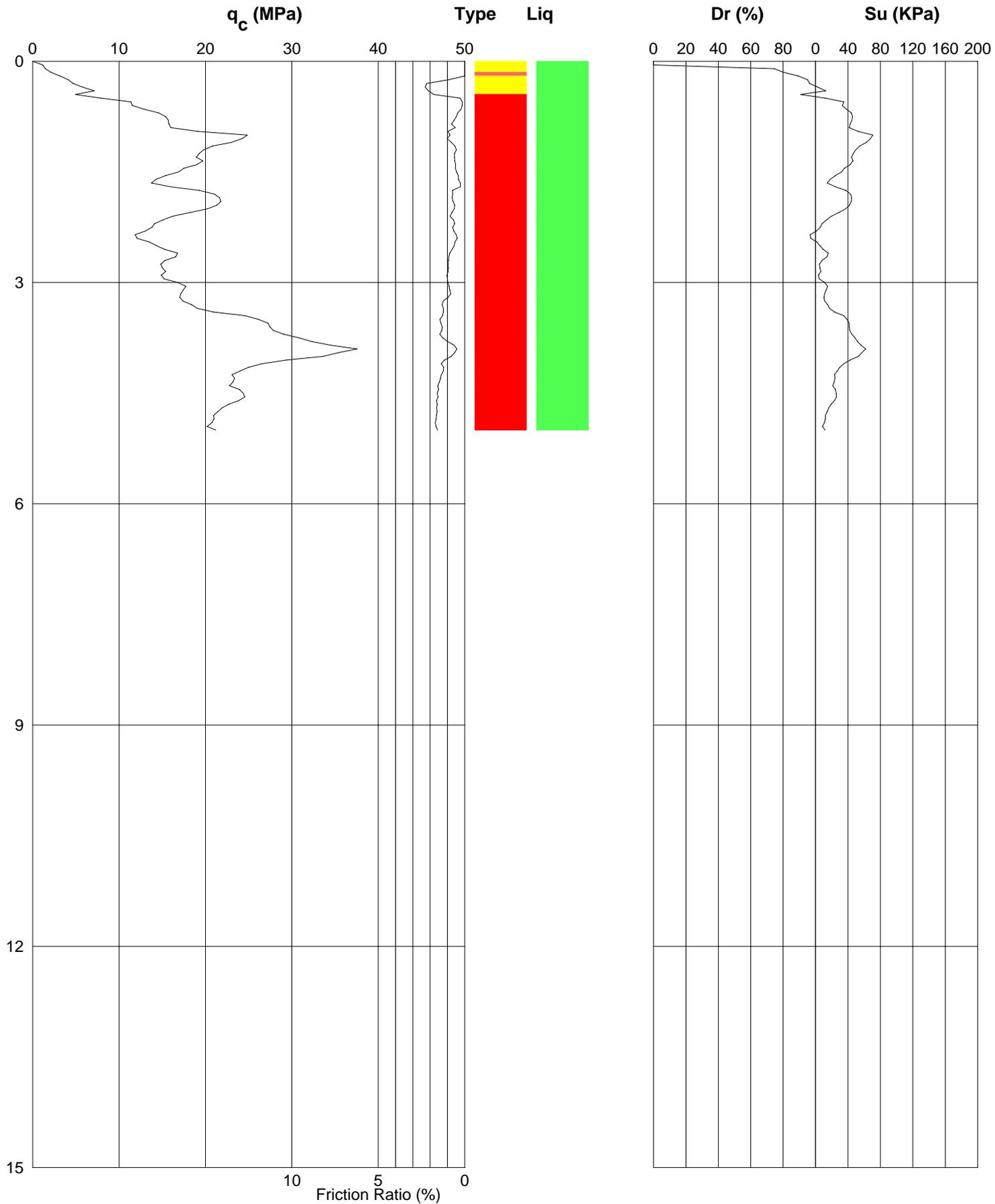
Location: Jacks Point, Queenstown

Date: 26-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

CPT No: 215

Project: Tonkin & Taylor Ltd

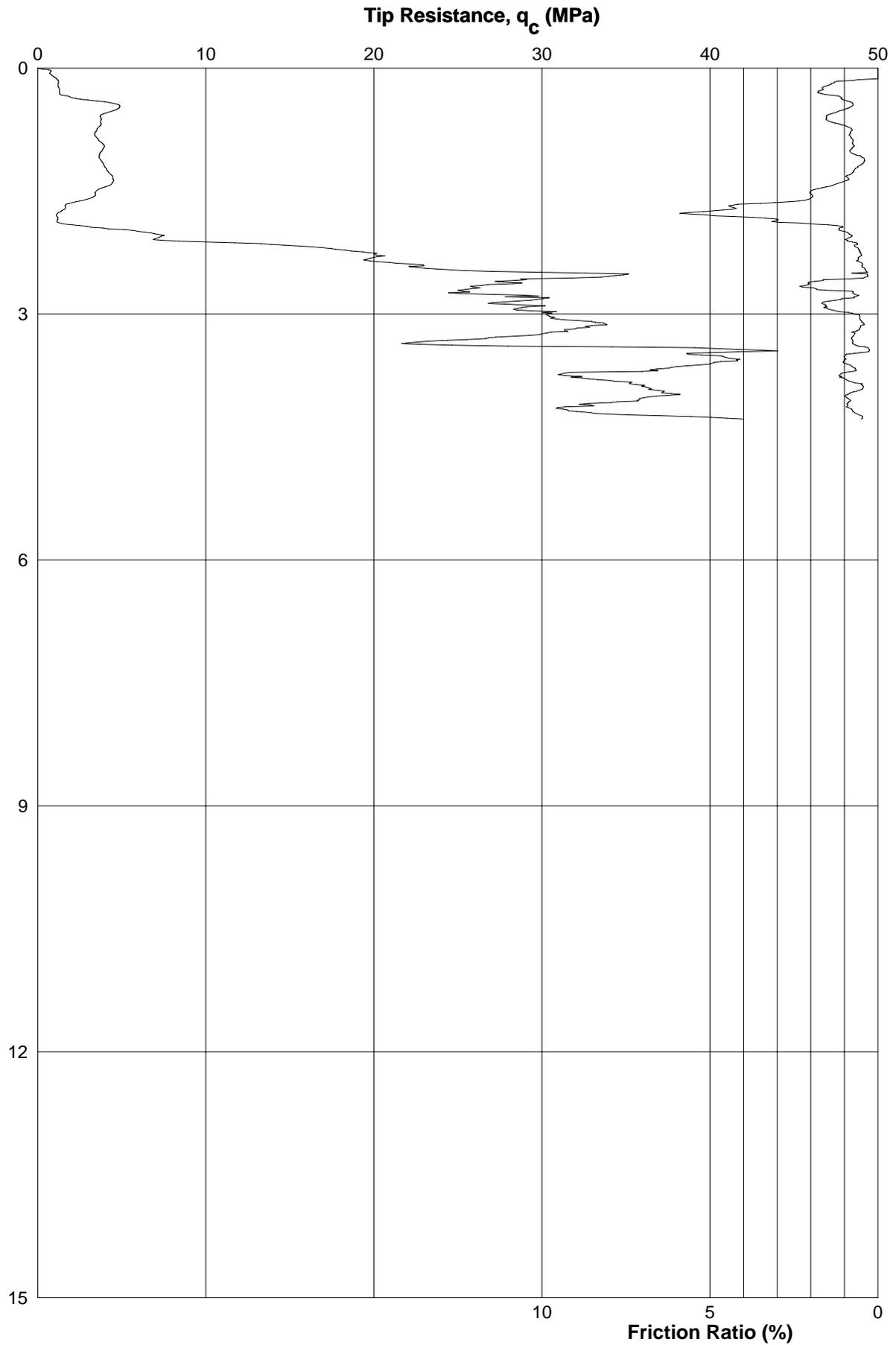
Location: Jacks Point, Queenstown

Date: 26-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 216

Project: Tonkin & Taylor Ltd

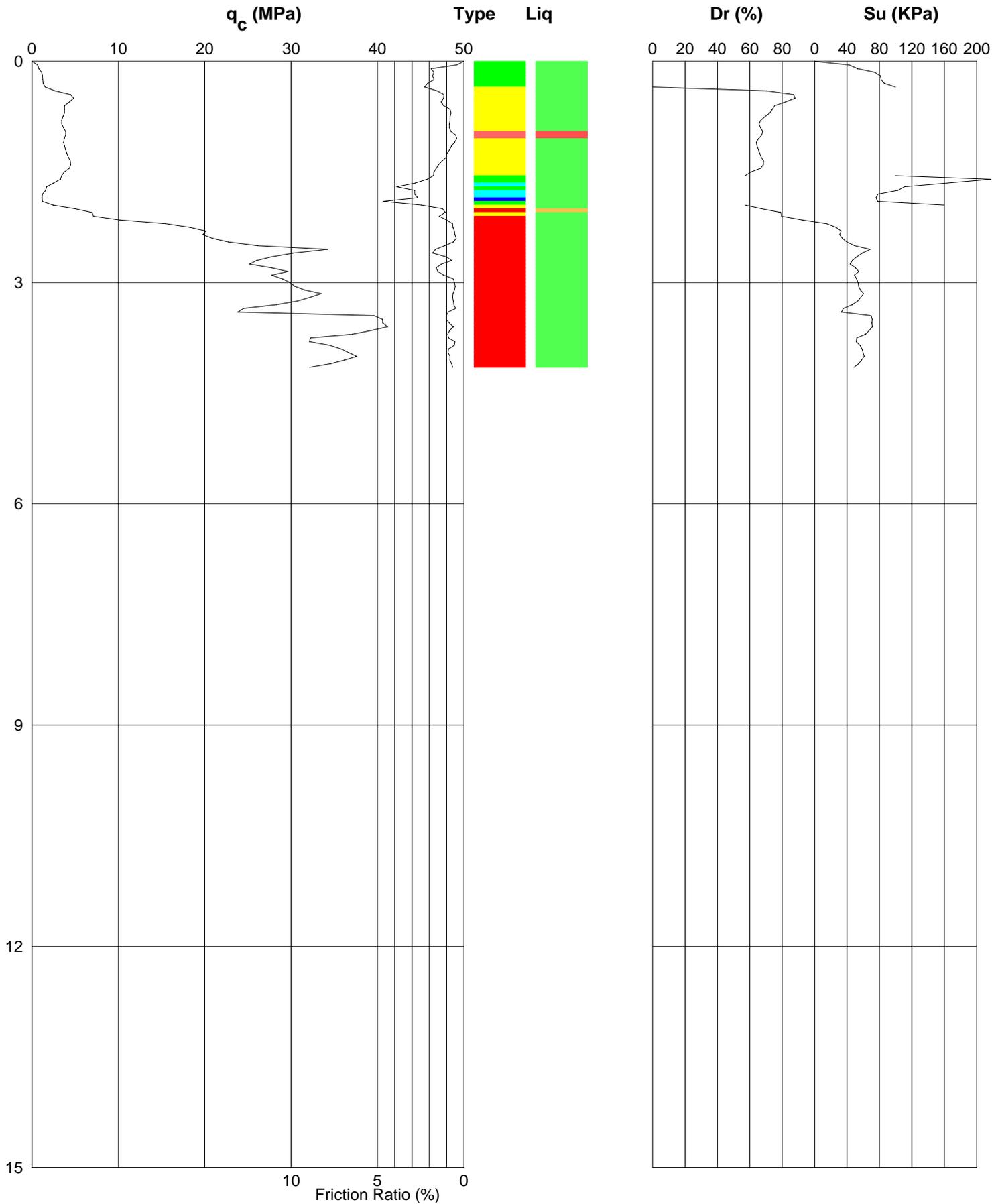
Location: Jacks Point, Queenstown

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Operator: J.Harvey

Remark: Effective Refusal

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Job No: 4934

CPT No: 216

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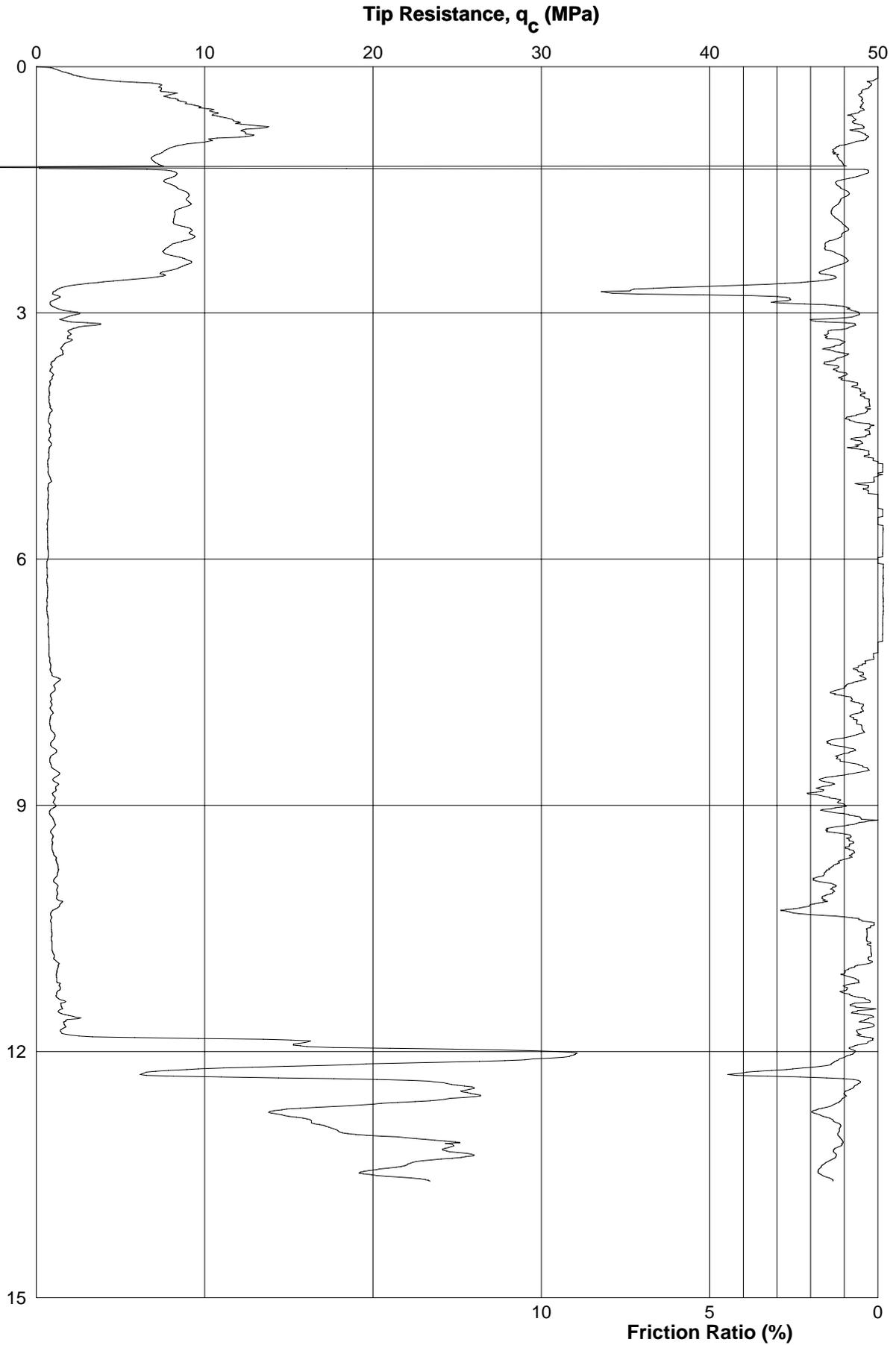
Location: Jacks Point, Queenstown

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STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 217

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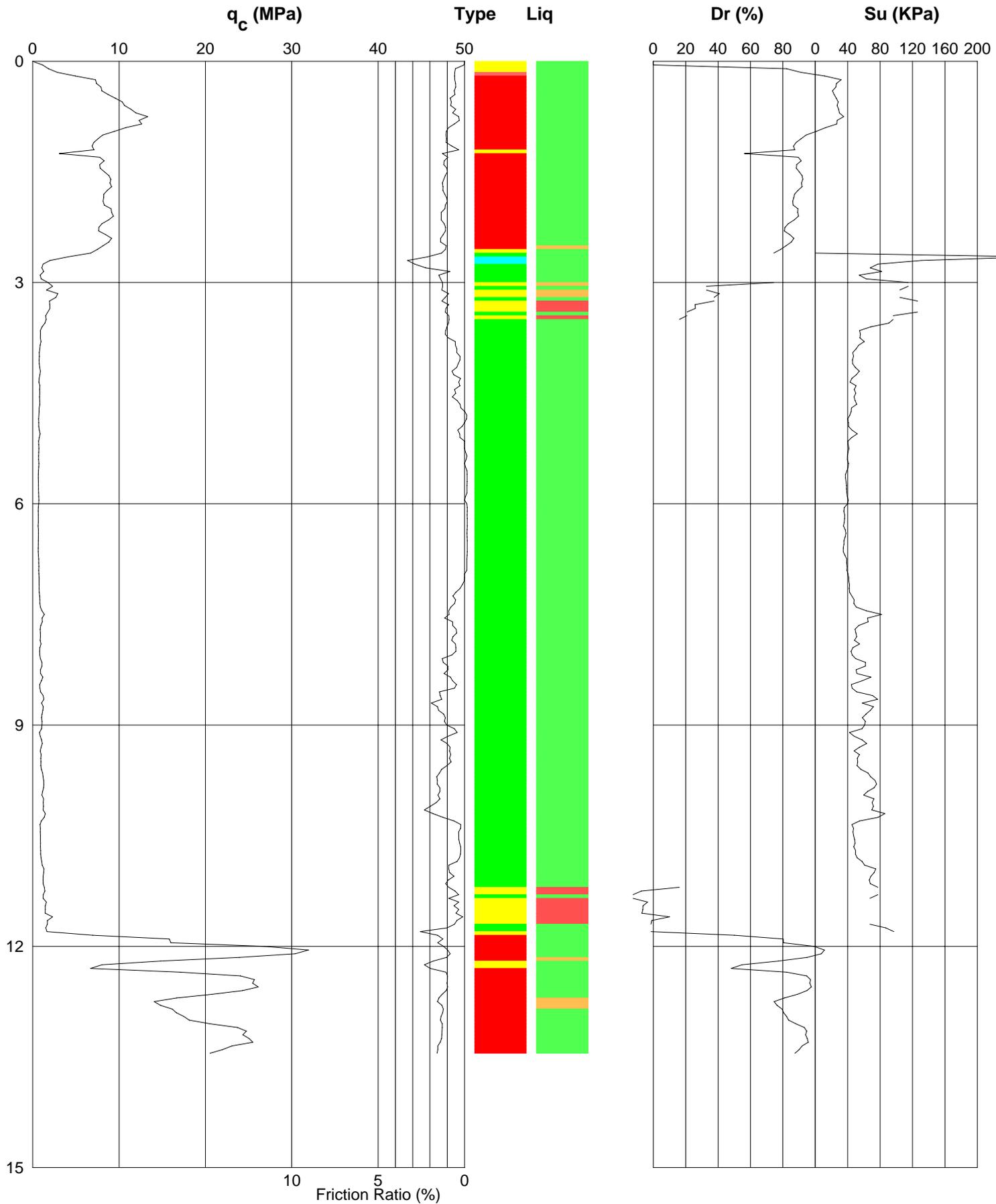
Location: Jacks Point, Queenstown

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Job No: 4934

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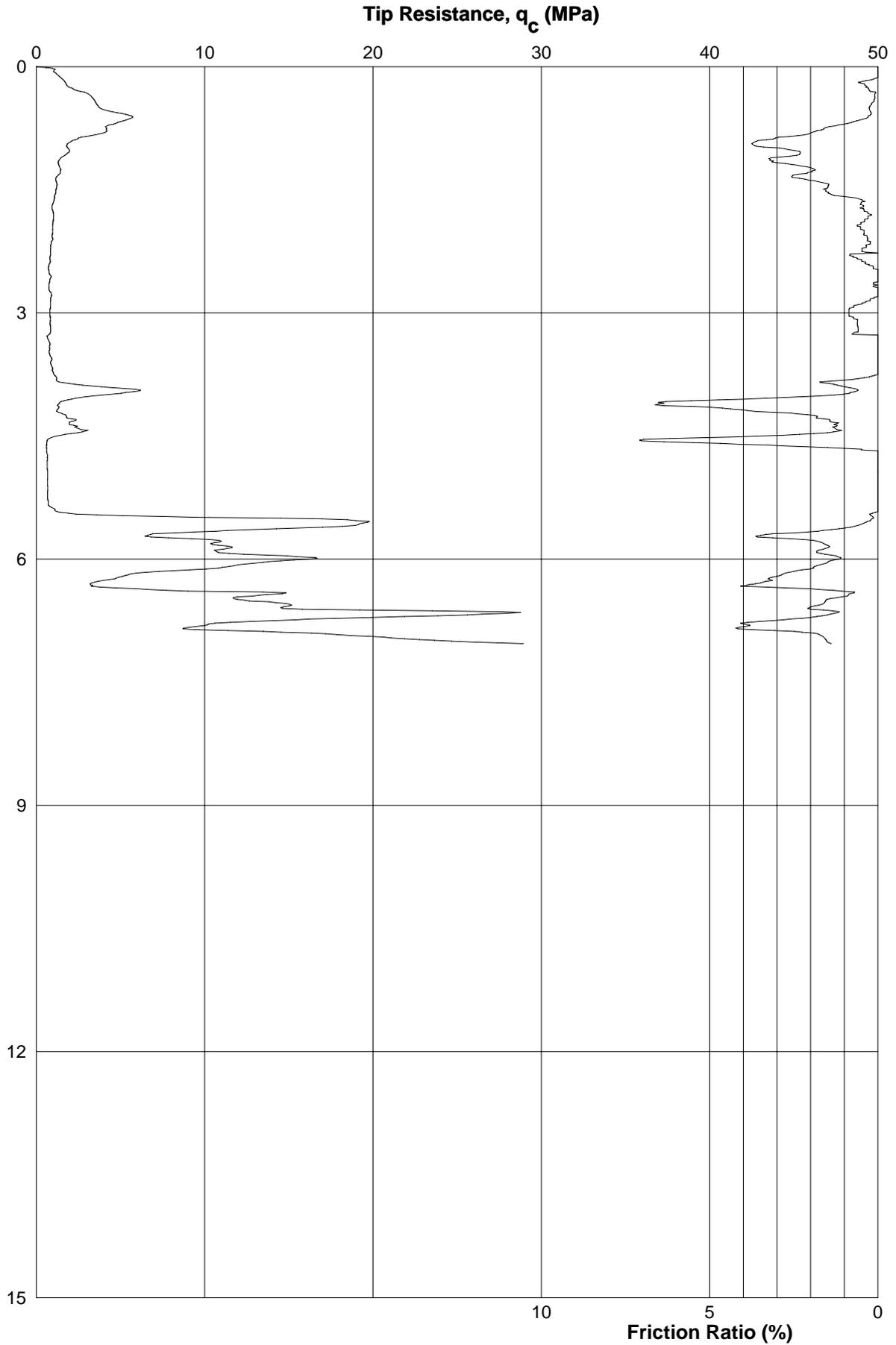
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Date: 26-9-07

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STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 218

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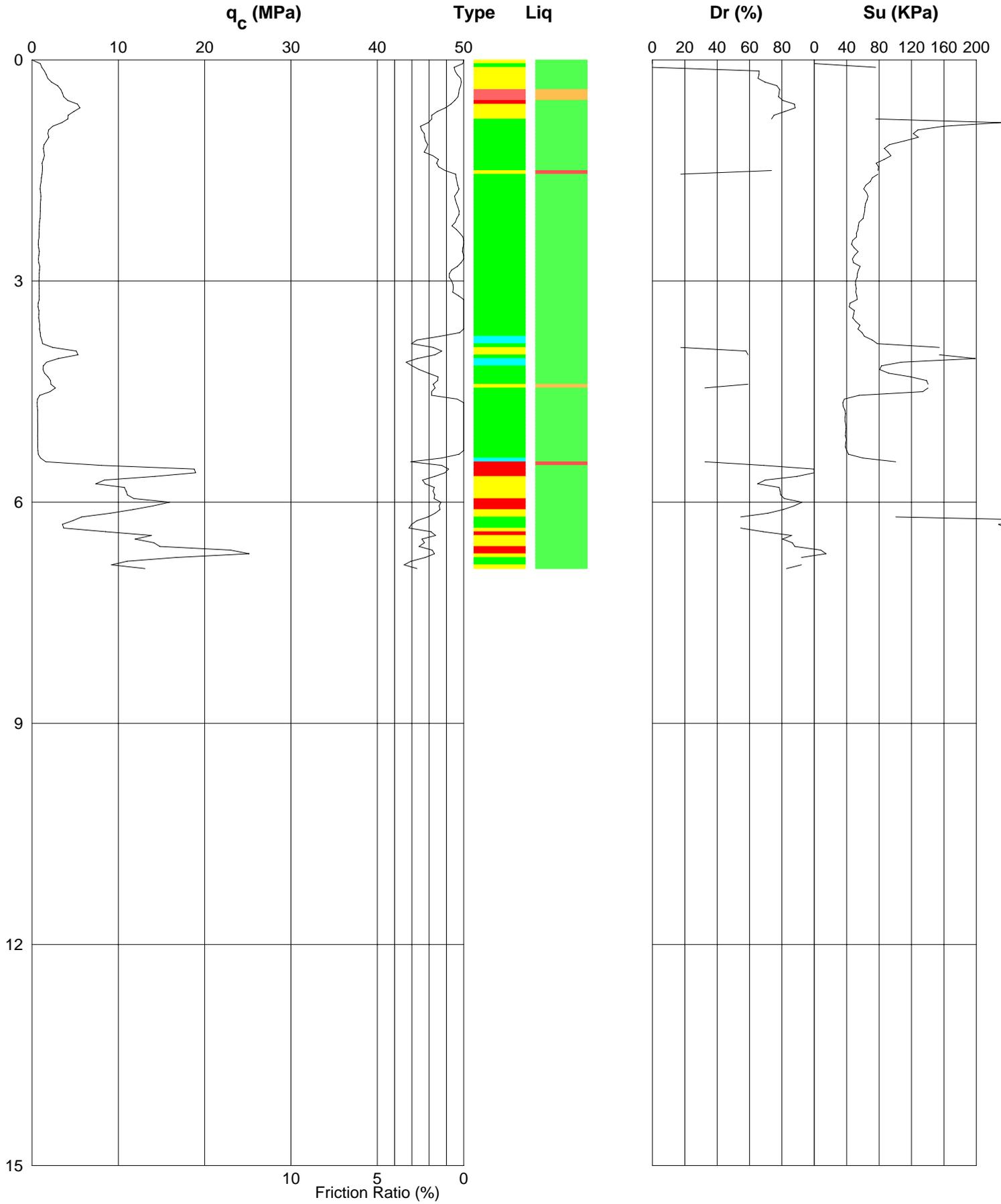
Location: Jacks Point, Queenstown

Date: 26-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

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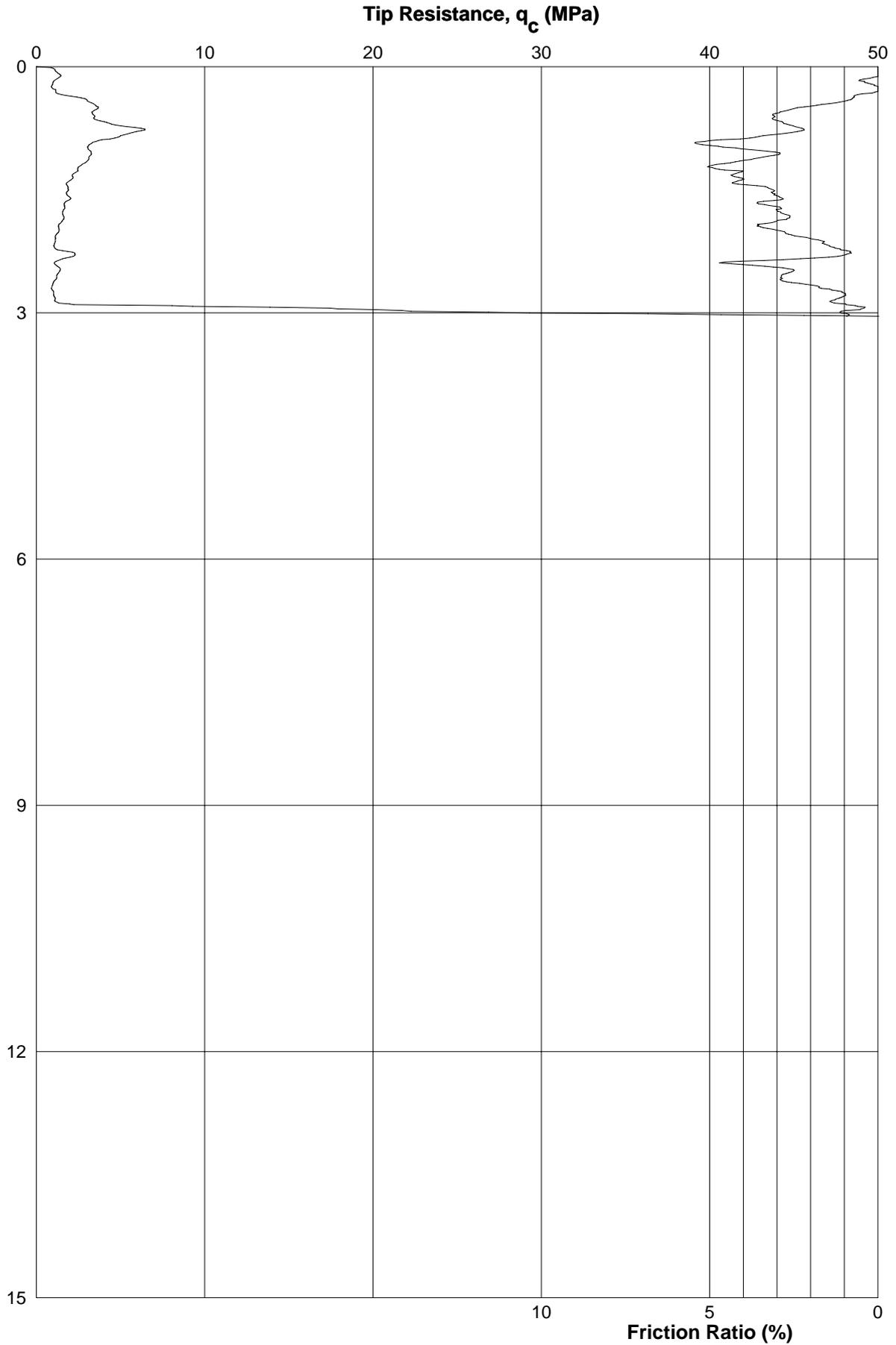
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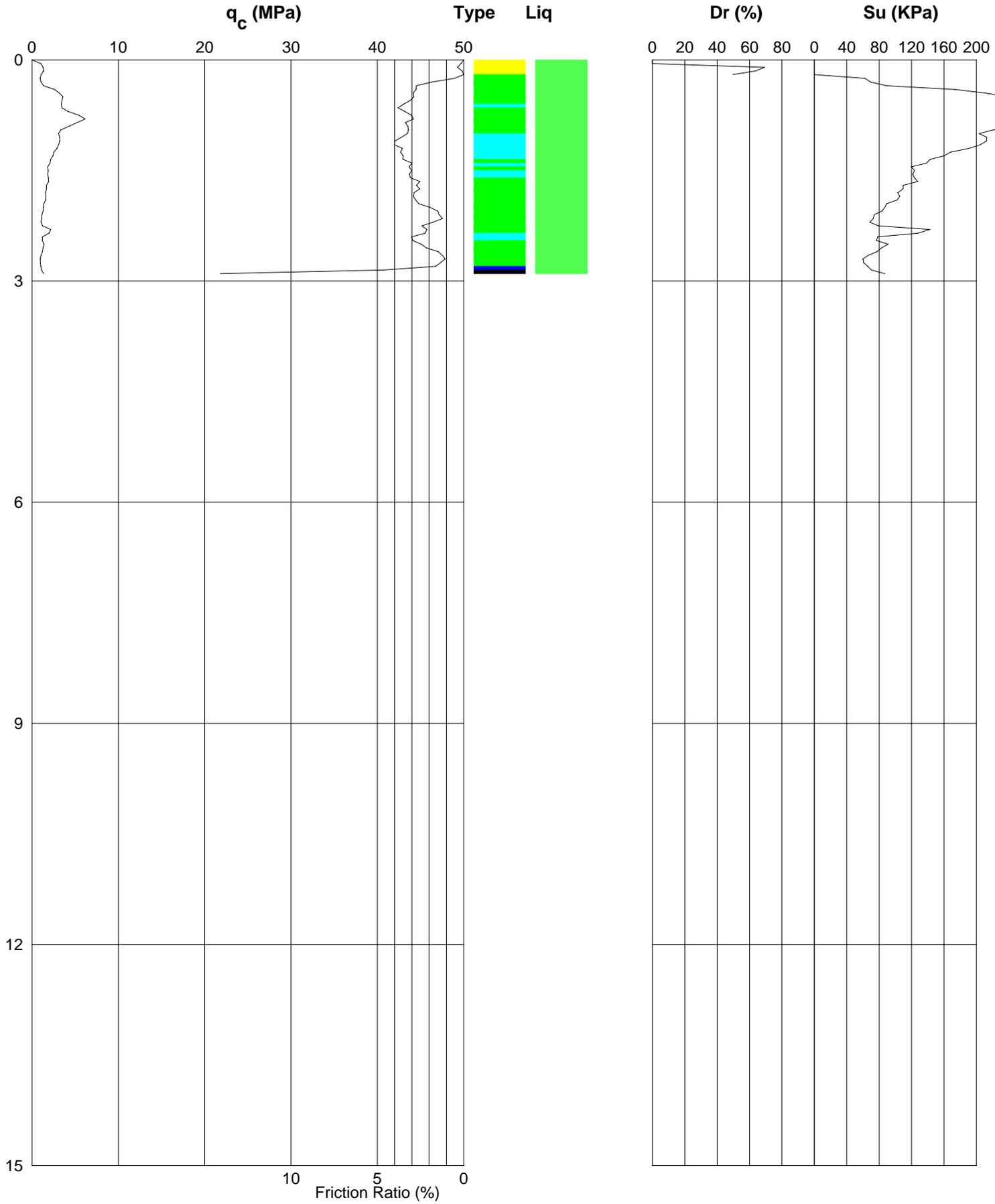
Location: Jacks Point, Queenstown

Date: 26-9-07

Operator: J.Harvey

Remark: Effective Refusal

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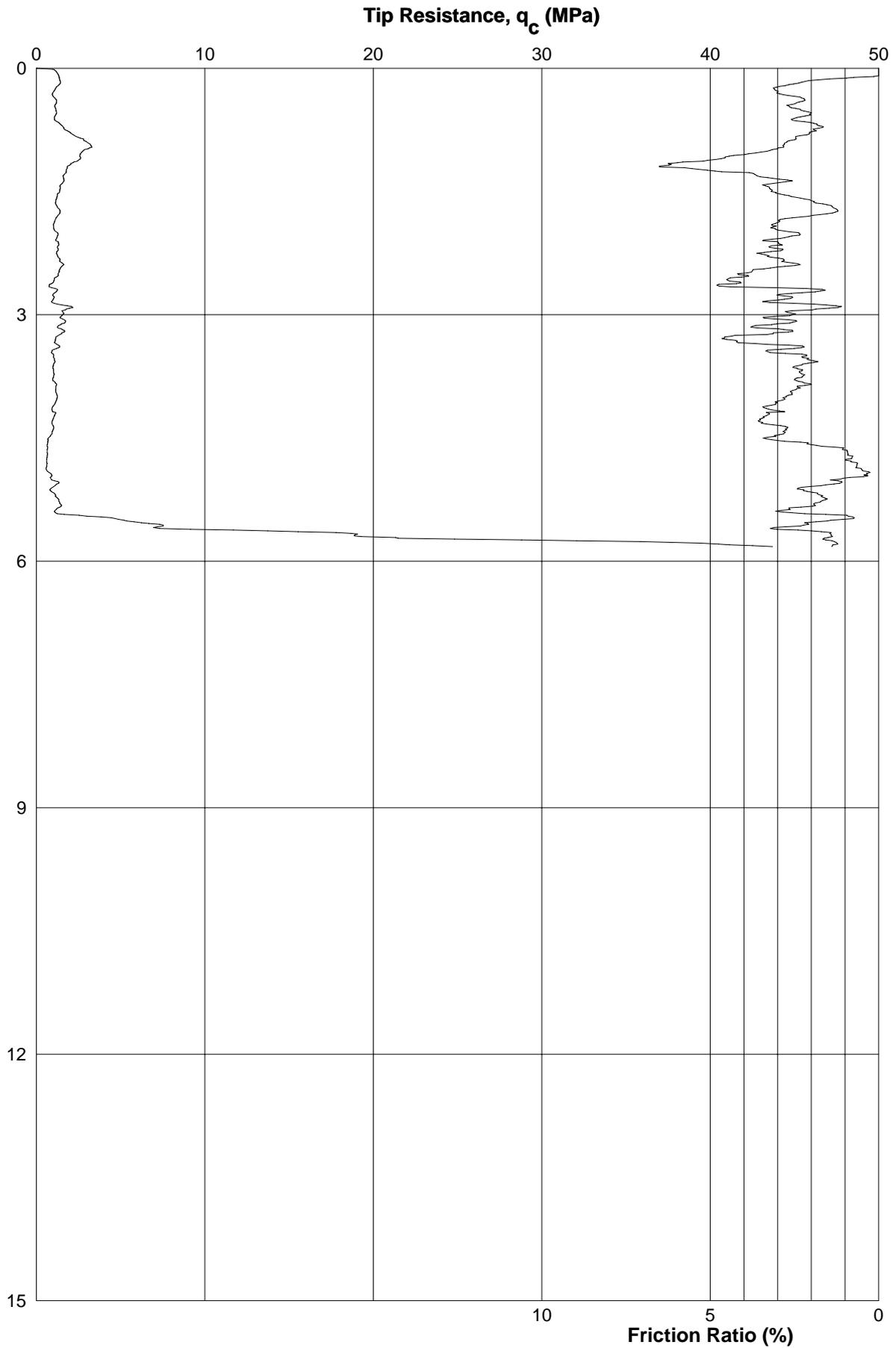
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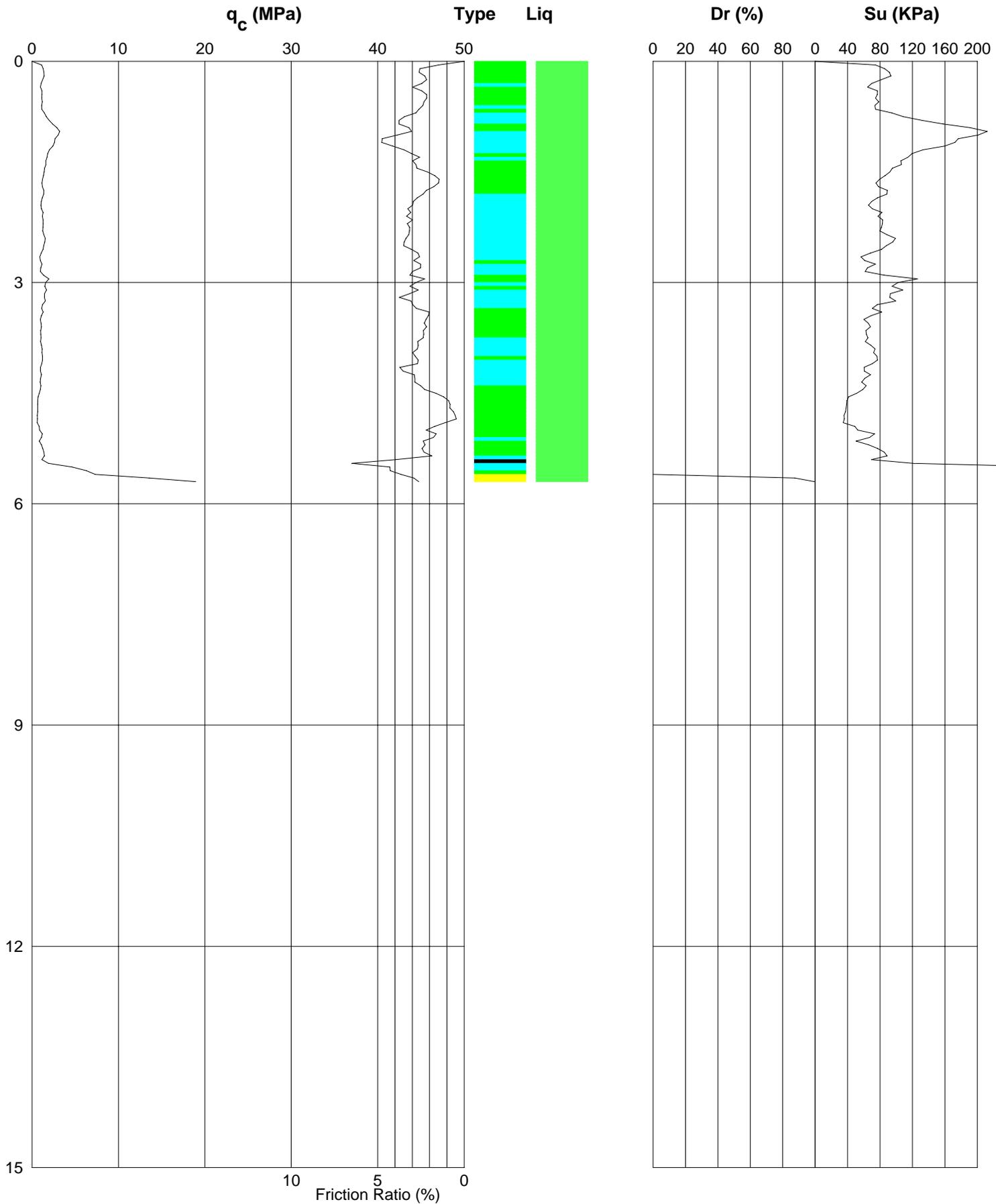
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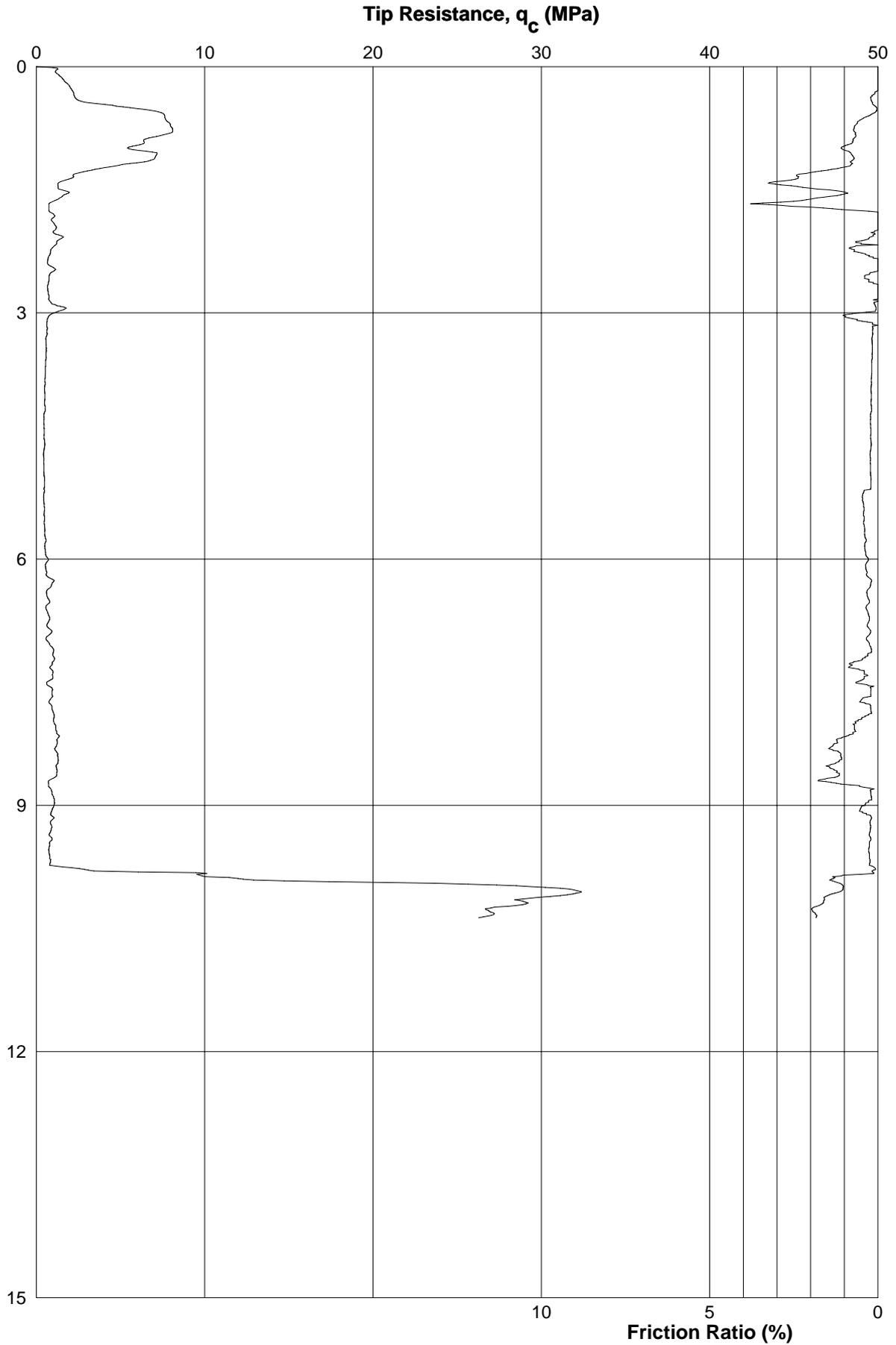
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Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 221

Project: Tonkin & Taylor Ltd

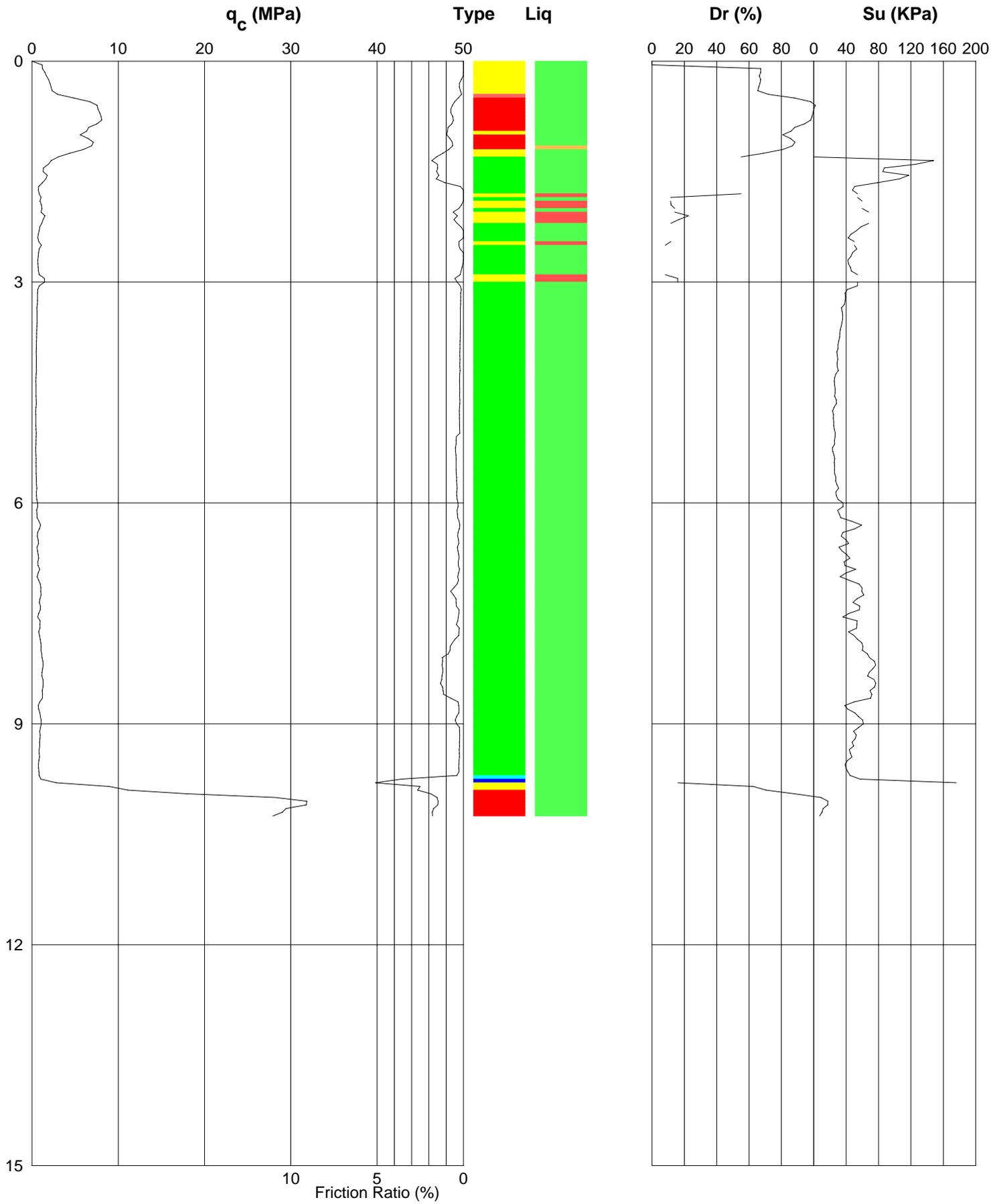
Location: Jacks Point, Queenstown

Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

CPT No: 221

Project: Tonkin & Taylor Ltd

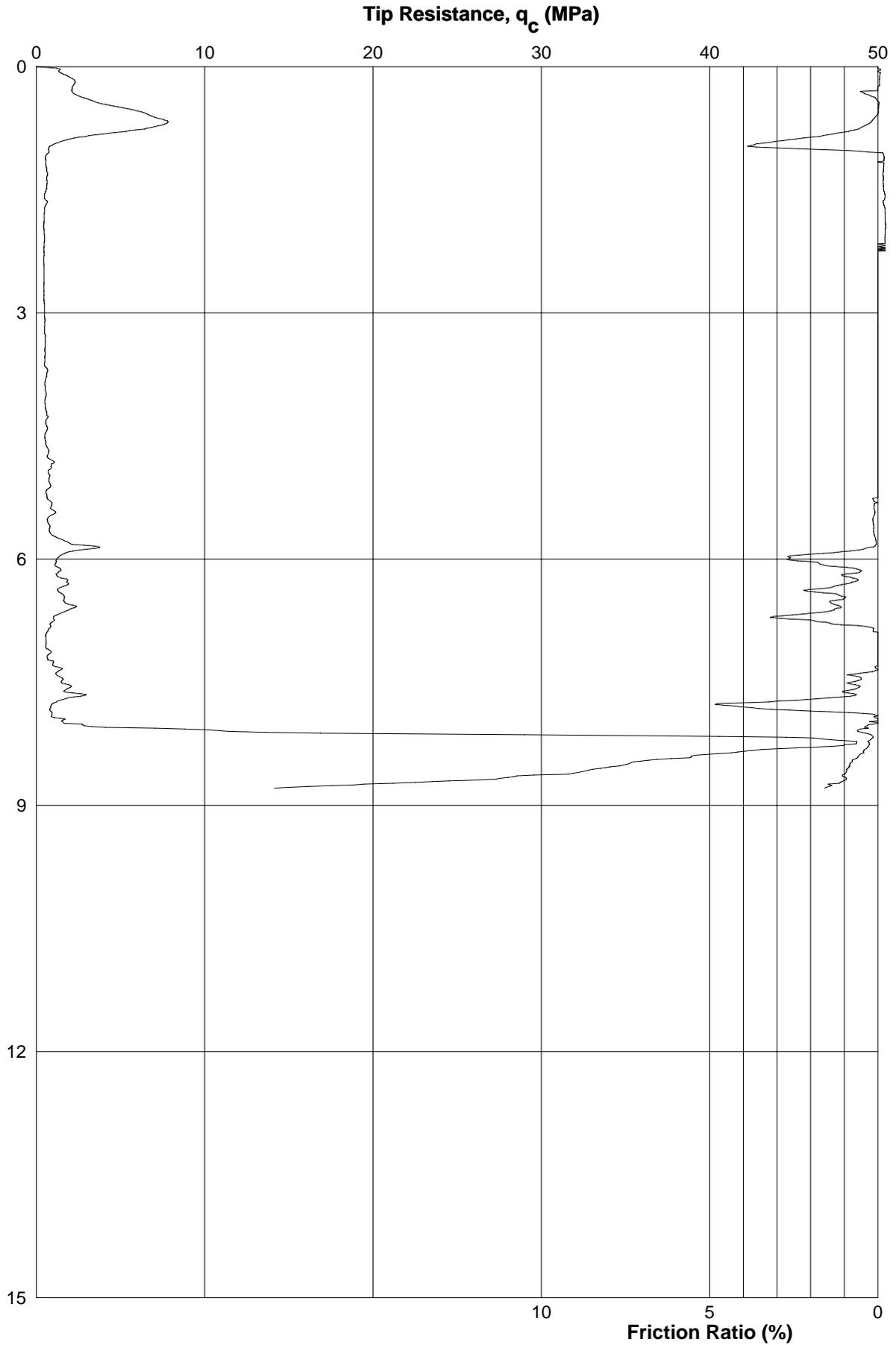
Location: Jacks Point, Queenstown

Date: 27-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 222

Project: Tonkin & Taylor Ltd

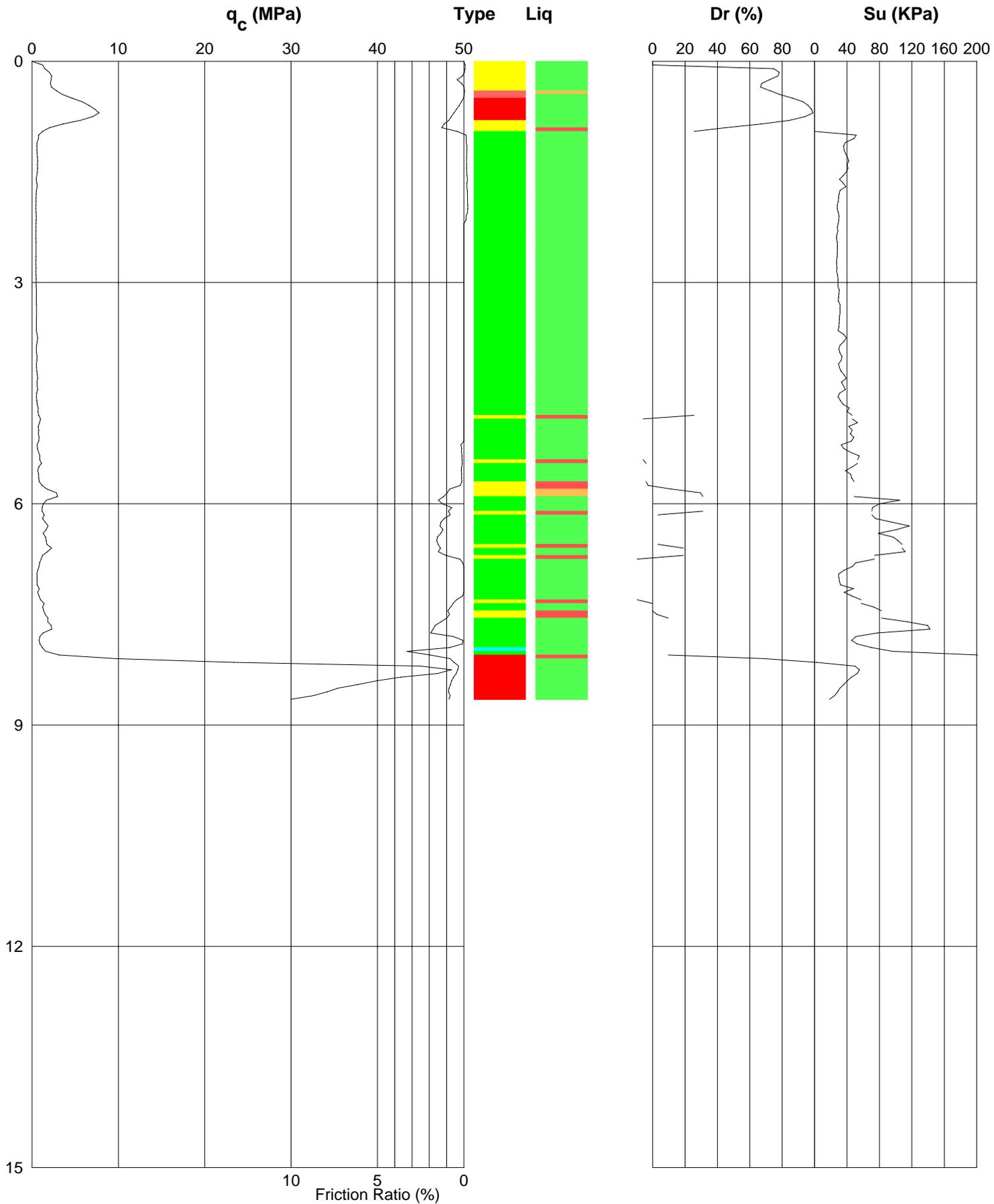
Location: Jacks Point, Queenstown

Date: 28-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

CPT No: 222

Project: Tonkin & Taylor Ltd

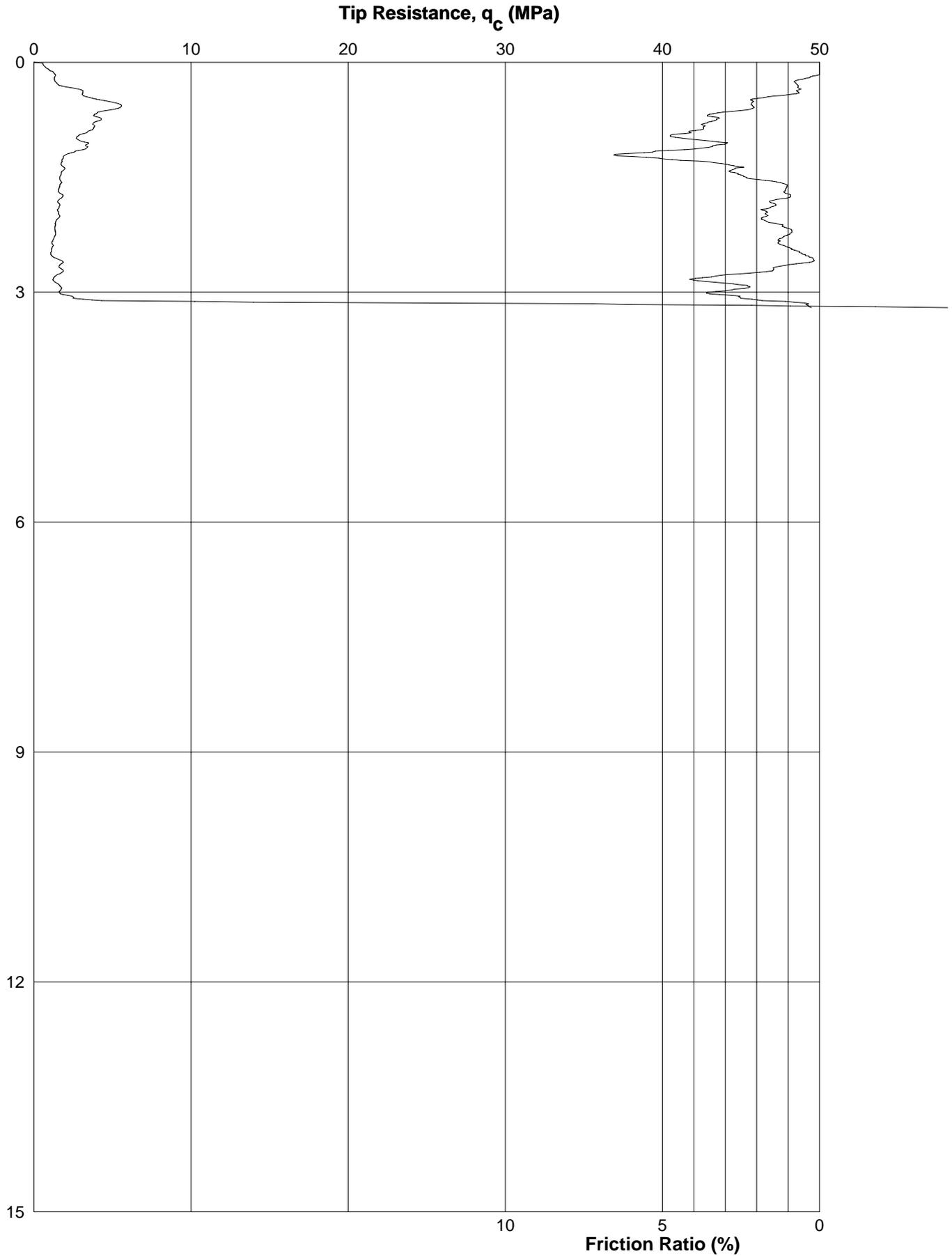
Location: Jacks Point, Queenstown

Date: 28-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) REPORT



Job No: 4934

CPT No: 223

Project: Tonkin & Taylor Ltd

Location: Jacks Point, Queenstown

Date: 28-9-07

Operator: J.Harvey

Remark: Effective Refusal

STANDARD CONE PENETROMETER TEST (CPT) INTERPRETIVE REPORT



Job No: 4934

CPT No: 223

Project: Tonkin & Taylor Ltd

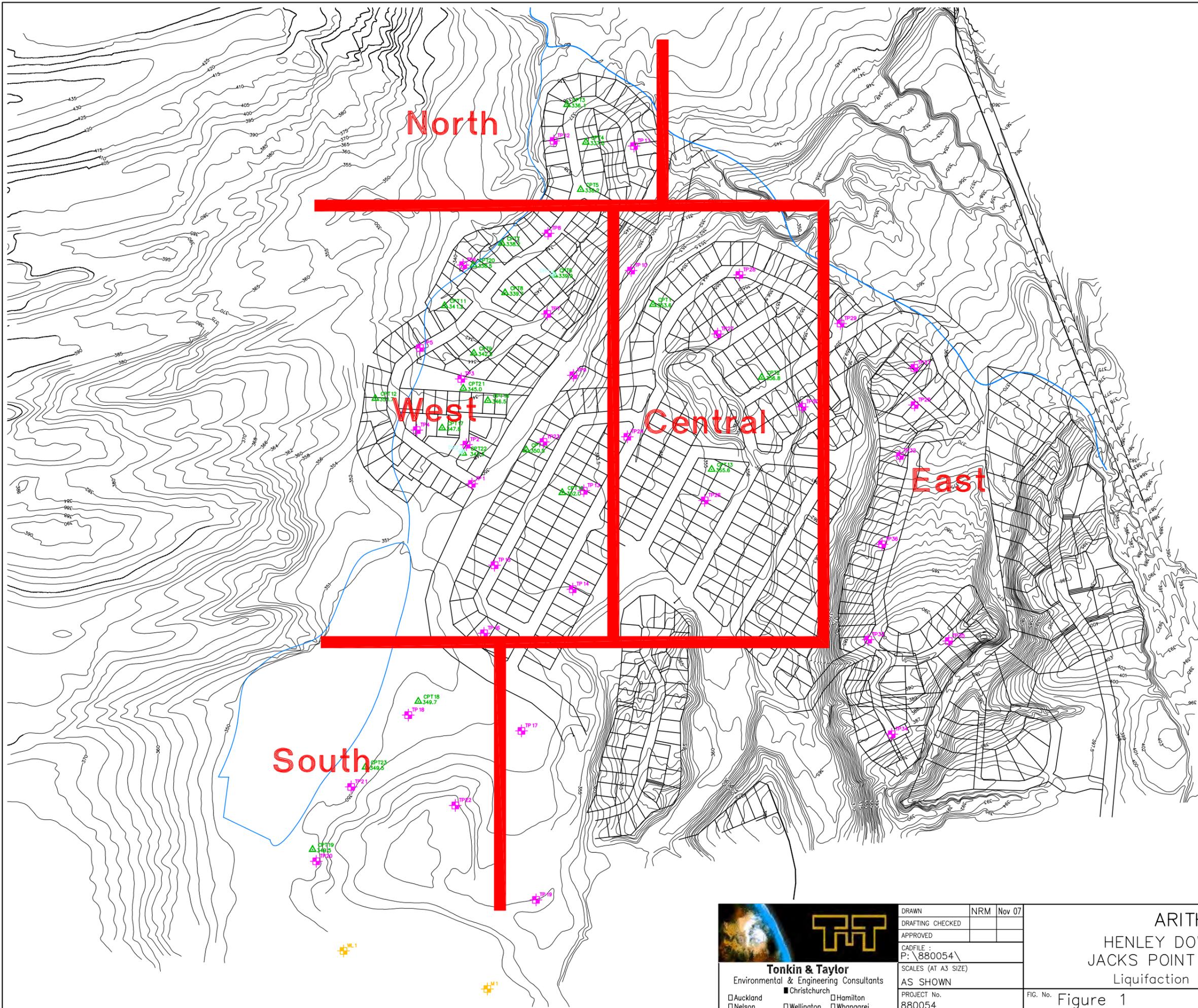
Location: Jacks Point, Queenstown

Date: 28-9-07

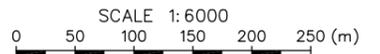
Operator: J.Harvey

Remark: Effective Refusal

Appendix E: Liquefaction Site Plan



| Predicted Settlement (mm) | | |
|---------------------------|-----|-----|
| Location | SLS | ULS |
| North | – | 10 |
| West | 30 | 80 |
| Central | – | 5 |
| East | – | – |
| South | 40 | 65 |



Tonkin & Taylor
Environmental & Engineering Consultants

Auckland Christchurch Hamilton
 Nelson Wellington Whangarei

| | | |
|------------------|------------|--------|
| DRAWN | NRM | Nov 07 |
| DRAFTING CHECKED | | |
| APPROVED | | |
| CADFILE : | P:\880054\ | |
| PROJECT No. | 880054 | |

ARITH LIMITED
 HENLEY DOWNS SUBDIVISION
 JACKS POINT – HENLEY DOWNS
 Liquefaction Potential Site Plan

FIG. No. **Figure 1** REV. **0**

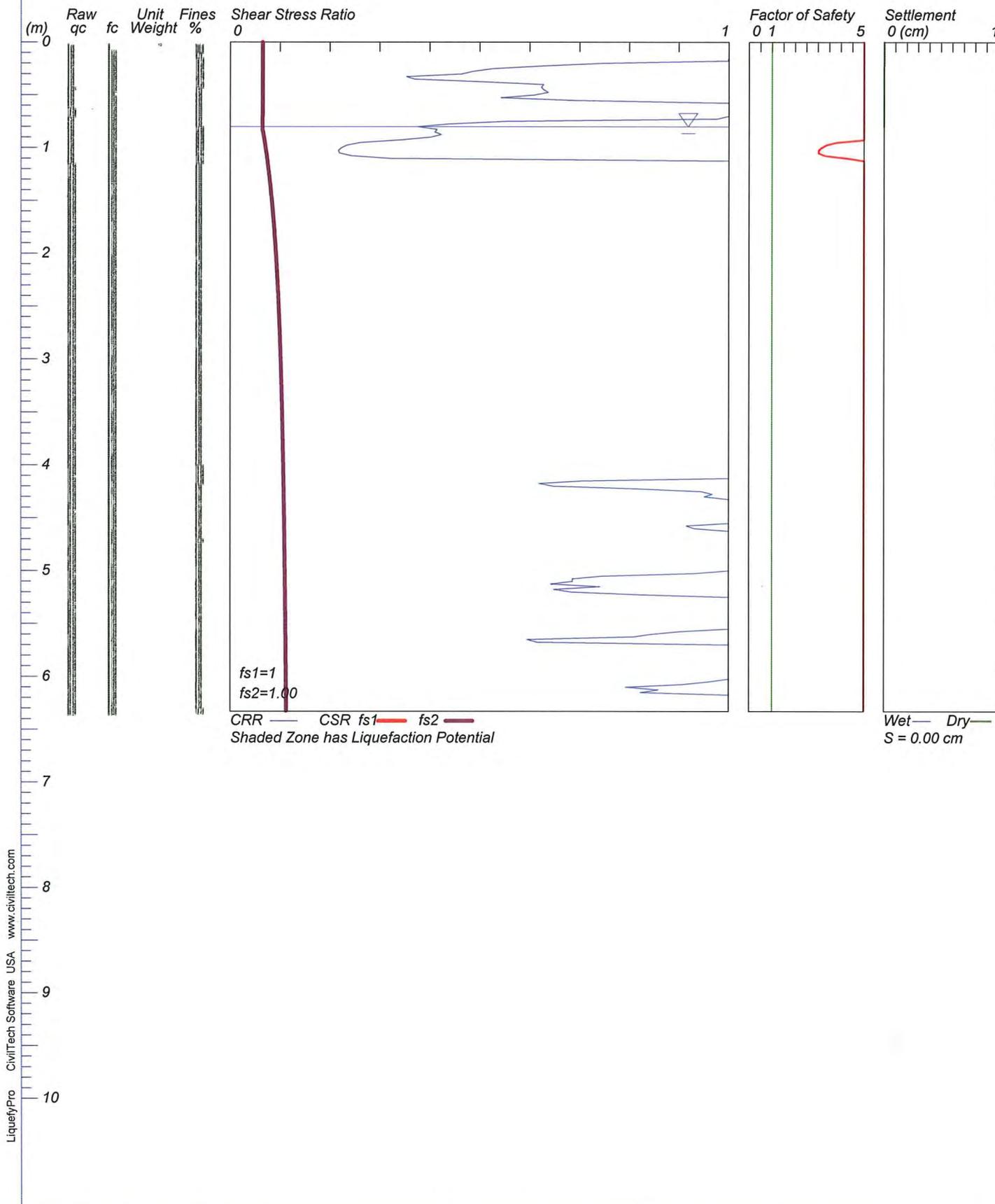
Appendix F: Liquefaction Analysis

LIQUEFACTION ANALYSIS

JACKS POINT - SLS

Hole No.=01 Water Depth=0.8 m Surface Elev.=353.6

Magnitude=7.0
Acceleration=0.10g



LiquefyPro CivilTech Software USA www.civiltch.com

LIQUEFACTION ANALYSIS

JACKS POINT - SLS

Hole No.=02 Water Depth=0.8 m Surface Elev.=356.8

Magnitude=7.0
Acceleration=0.10g

